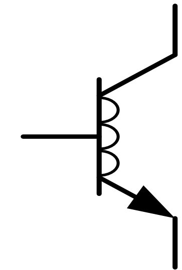
EE 330
Lecture 28

Two-Port Amplifier Models

Relative Magnitude of Small Signal BJT Parameters

$$g_m = \frac{I_{CQ}}{V_t} \qquad g_\pi = \frac{I_{CQ}}{\beta V_t} \qquad g_o \cong \frac{I_{CQ}}{V_{AF}}$$



$$\frac{g_m}{g_\pi} = \frac{\left[\frac{I_Q}{V_t}\right]}{\left[\frac{I_Q}{\beta V_t}\right]}$$

$$\frac{g_\pi}{g_o} = \frac{\left[\frac{I_Q}{\beta V_t}\right]}{\left[\frac{I_Q}{V_{AF}}\right]}$$

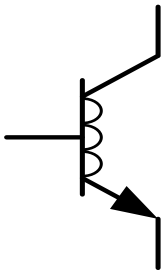
for vertical npn

$$g_m >> g_\pi >> g_o$$

Often the g_o term can be neglected in the small signal model because it is so small

Relative Magnitude of Small Signal BJT Parameters

$$g_m = \frac{I_{CQ}}{V_t} \qquad g_\pi = \frac{I_{CQ}}{\beta V_t} \qquad g_o \cong \frac{I_{CQ}}{V_{AF}}$$



$$\frac{g_m}{g_\pi} = \frac{\left[\frac{I_Q}{V_t}\right]}{\left[\frac{I_Q}{\beta V_t}\right]} = \beta$$

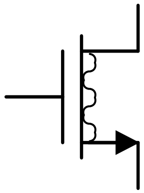
for vertical npn

$$g_m >> g_\pi >> g_o$$

$$\frac{g_\pi}{g_o} = \frac{\left[\frac{I_Q}{\beta V_t}\right]}{\left[\frac{I_Q}{V_{AF}}\right]} = \frac{V_{AF}}{\beta V_t} \approx \frac{200\text{V}}{100 \bullet 26\text{mV}} = 77$$

- **Often the g_o term can be neglected in the small signal model because it is so small**
- **Be careful about neglecting g_o prior to obtaining a final expression**

How does g_m vary with I_{DQ}?



$$g_m = \sqrt{\frac{2\mu C_{OX} W}{L}} \sqrt{I_{DQ}}$$

Varies with the square root of I_{DQ}

$$g_m = \frac{2I_{DQ}}{V_{GSQ} - V_T} = \frac{2I_{DQ}}{V_{EBQ}}$$

Varies linearly with I_{DQ}

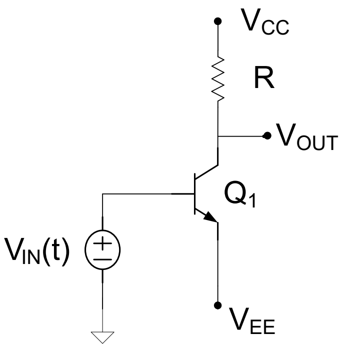
$$g_m = \frac{\mu C_{OX} W}{L}\left(V_{GSQ} - V_T\right)$$

Doesn't vary with I_{DQ}

Review from Previous Lecture

Large and Small Signal Parameter Domains

BJT



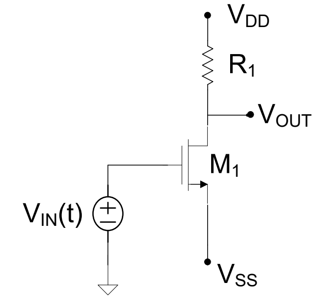
$$A_{VB} = -\frac{I_{CQ}R_1}{V_t}$$

$$A_V = -g_m R$$

MOSFET

$$A_{VM} = \frac{2I_{DQ}R}{[V_{SS} + V_T]}$$

$$A_V = -g_m R$$



Large Signal Parameter Domain: Quiescent Port and Model Variables

(No small-signal model parameters or small-signal port variables)

Small Signal Parameter Domain: Small-Signal Port and Model Variables

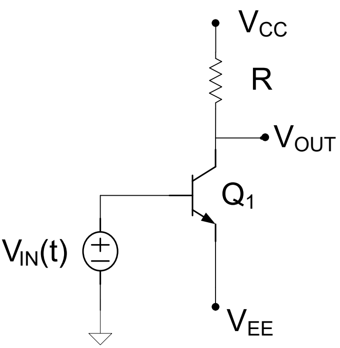
(No dc model parameters or dc port variables)

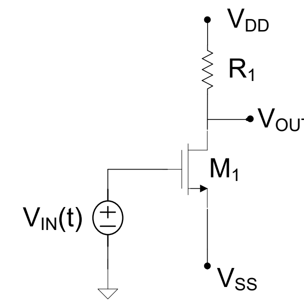
Review from Previous Lecture

Gains for MOSFET and BJT Circuits

BJT

MOSFET



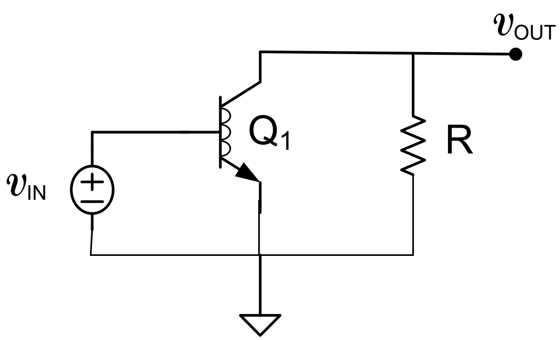


$$A_{VB} = -\frac{I_{CQ} R_1}{V_t}$$

Large Signal Parameter Domain
(If g_o is neglected)

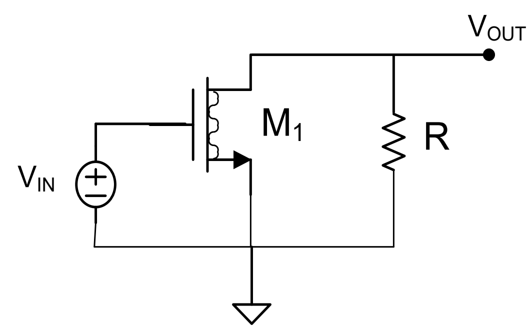
$$A_{VM} = \frac{2I_{DQ} R}{[V_{SS} + V_T]}$$

For both circuits



Small Signal Parameter Domain
(neglecting g_0)

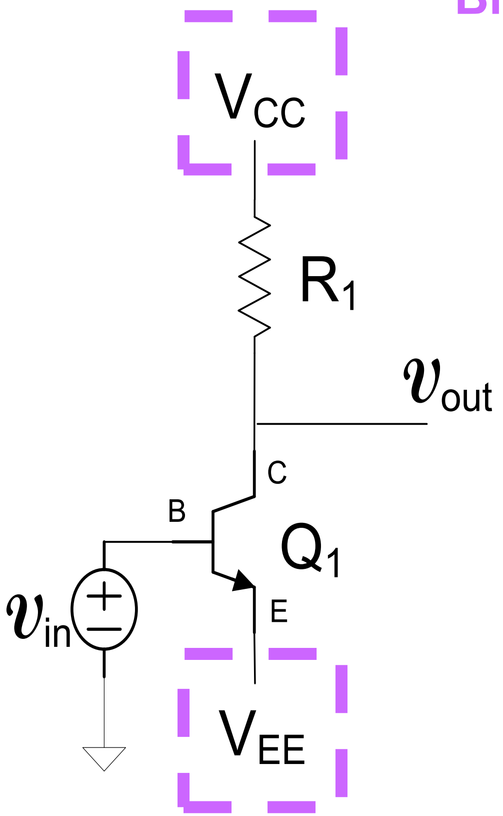
$$A_V = -g_m R$$

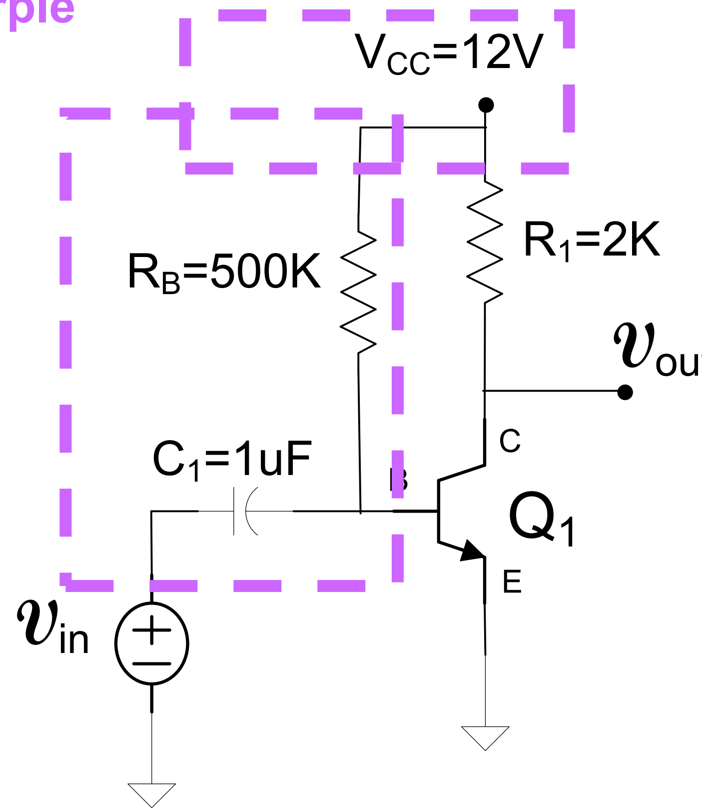


- Gains are identical in small-signal parameter domain !
- Gains vary linearly with small signal parameter g_m
- Power is often a key resource in the design of an integrated circuit
- In both circuits, power is proportional to I_{CQ} , I_{DQ} (if V_{SS} and V_{EE} are fixed)

Amplifier Biasing (precursor)

Biasing Circuits shown in purple





Not convenient to have multiple dc power supplies
V_{OUTQ} very sensitive to V_{EE}

Single power supply
Additional resistor and capacitor

- Small-Signal Analysis
  - Graphical Interpretation
  - MOSFET Model Extensions
  - Biasing (a precursor)

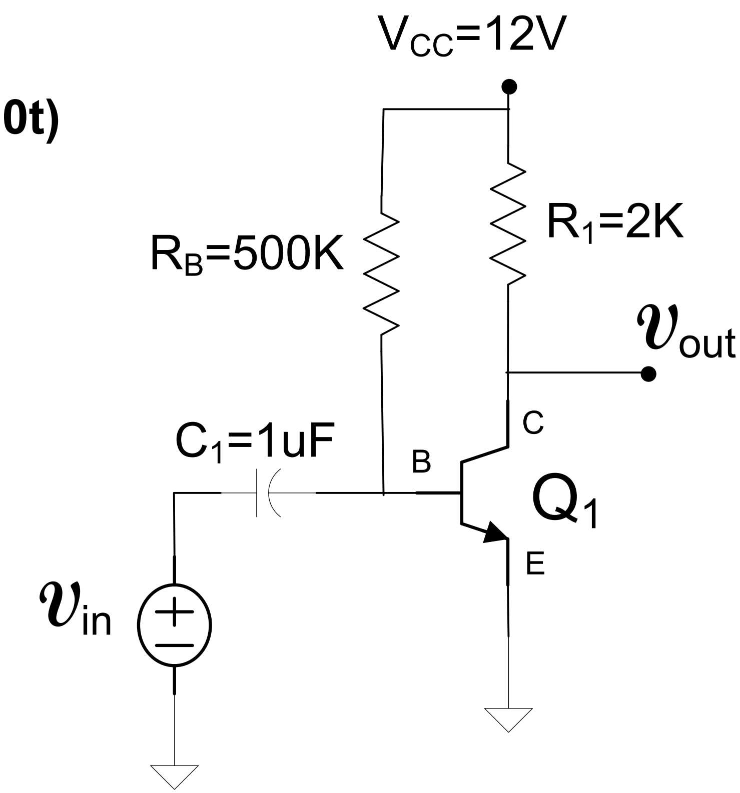
→ Two-Port Amplifier Modeling

Amplifier Characterization (an example)

This example serves as a precursor to amplifier characterization

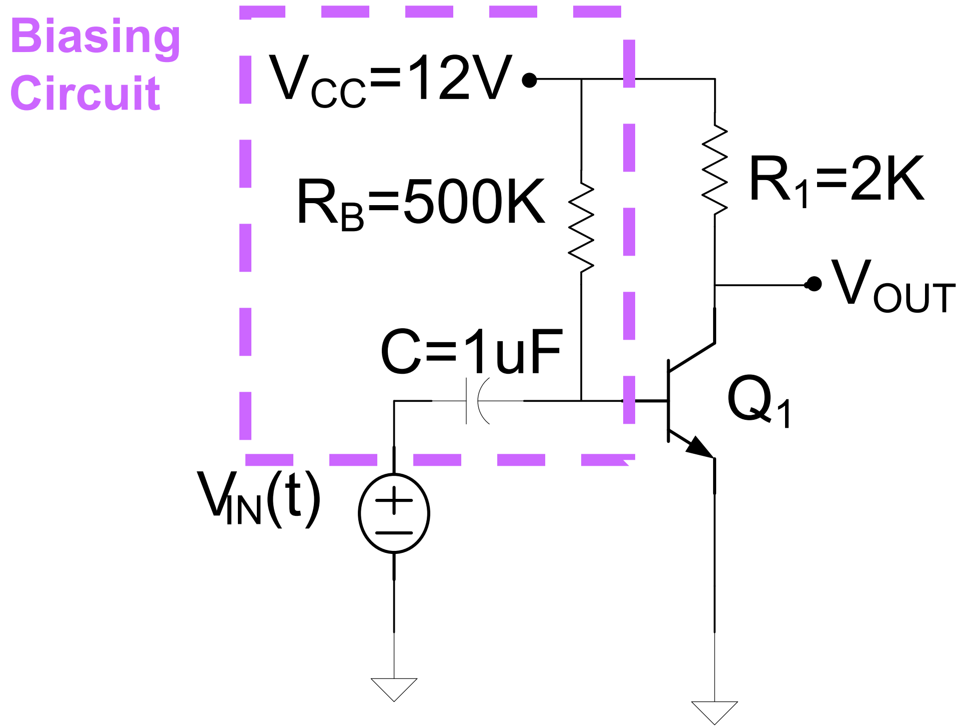
Determine V_{OUTQ}, A_V, R_{IN} Assume β=100

Determine v_{OUT} and $V_{OUT}(t)$ if v_{IN}=.002sin(400t)



In the following slides we will analyze this circuit

Amplifier Characterization (an example)



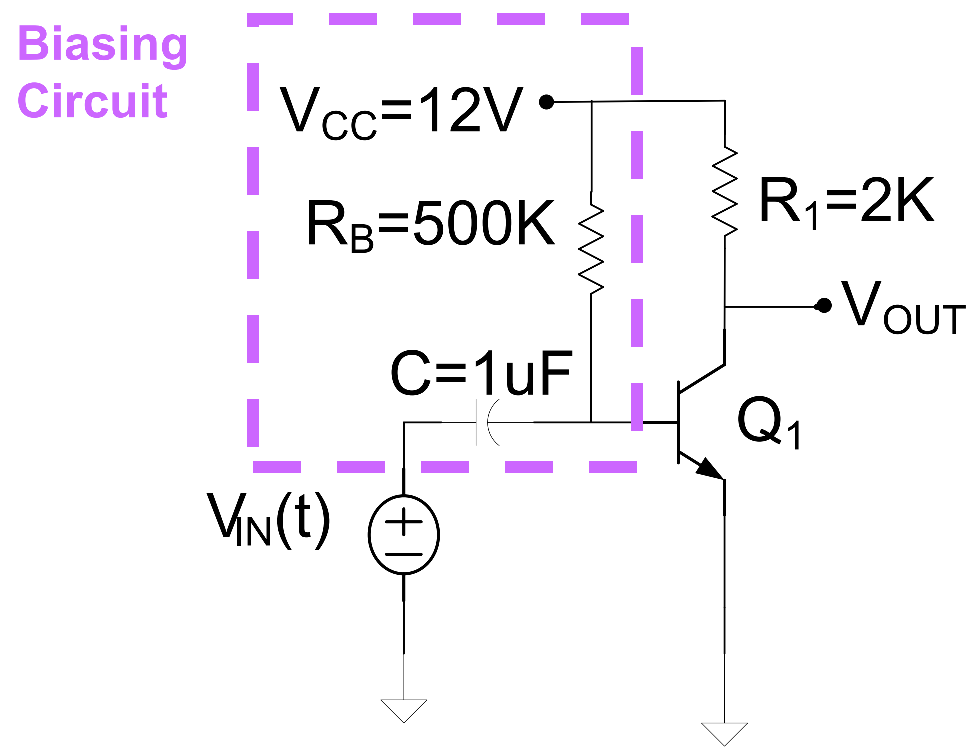
(biasing components: C, R_B, V_{CC} in this case, all disappear in small-signal voltage gain circuit)

(il general, all dc voltage sources, dc current sources, and large capacitors will disappear in small-signal analysis)

Several different biasing circuits can be used

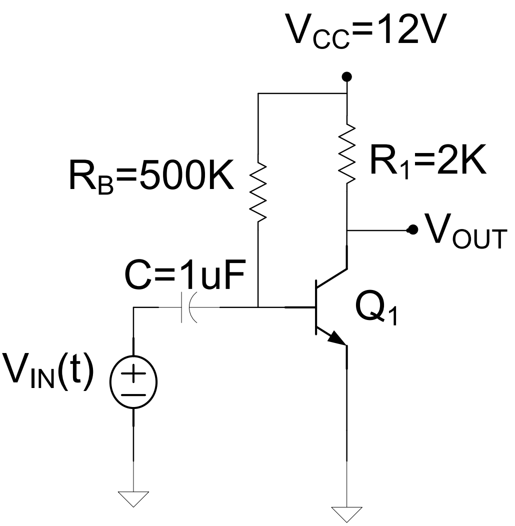
Amplifier Characterization (an example)

Determine V_{OUTQ}, A_V, R_{IN}

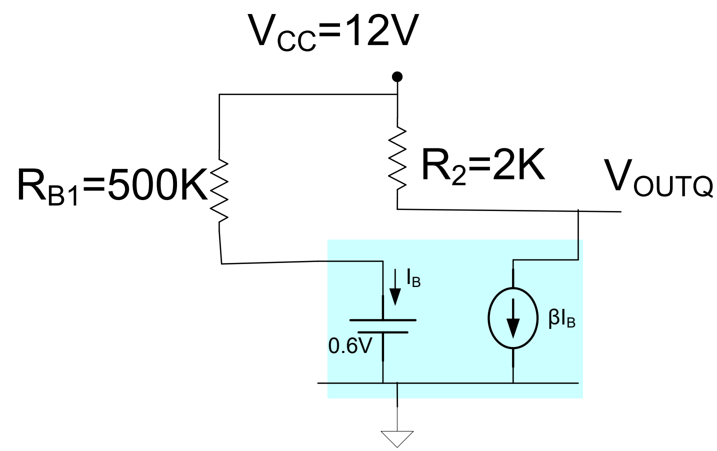


Amplifier Characterization (an example)

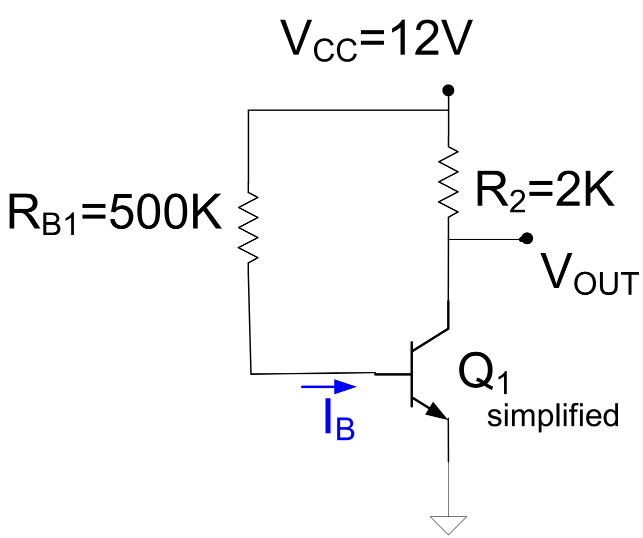
Determine V_{OUTQ}



β=100



dc equivalent circuit



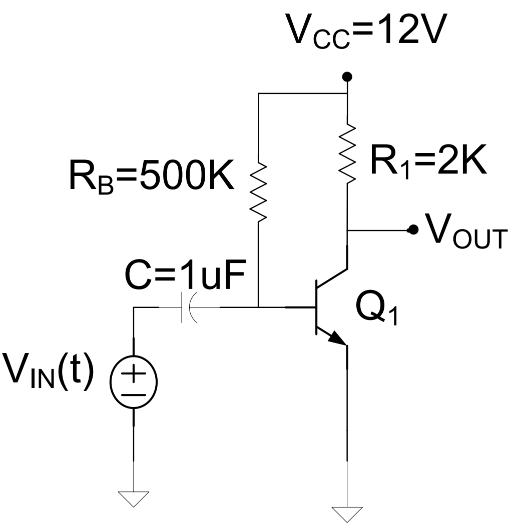
dc equivalent circuit

$$I_{CQ} = \beta I_{BQ} = 100\left(\frac{12V\text{-}0.6V}{500K}\right) = 2.3mA$$

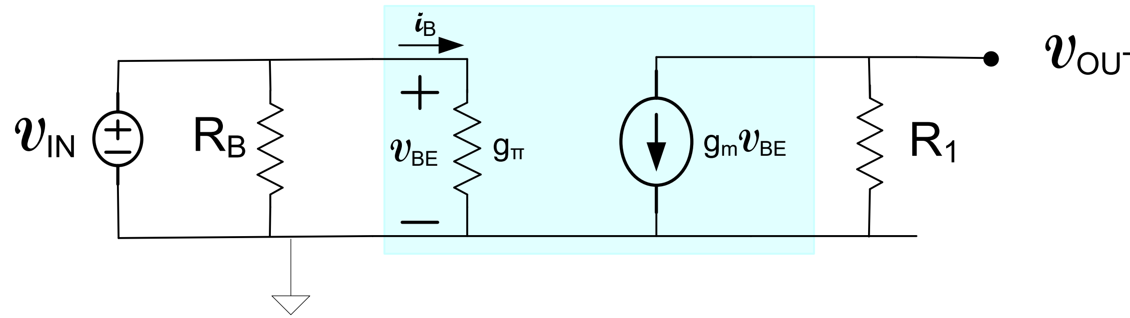
$$V_{OUTQ} = 12V\text{-}I_{CQ}R_1 = 12V - 2.3mA \bullet 2K = 7.4V$$

Amplifier Characterization (an example)

Determine the SS voltage gain (A_V)



β=100



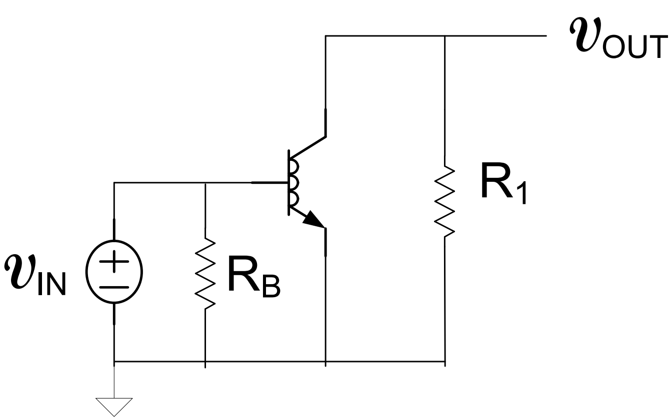
ss equivalent circuit

$$\left.\begin{array}{l} v_{OUT} = -g_m v_{BE} R_1 \\ v_{IN} = v_{BE} \end{array}\right\}$$

$$A_V = -R_1 g_m$$

$$A_V \cong -\frac{I_{CQ} R_1}{V_t}$$

$$A_V \cong -\frac{2.3\text{mA} \bullet 2\text{K}}{26\text{mV}} \cong -177$$

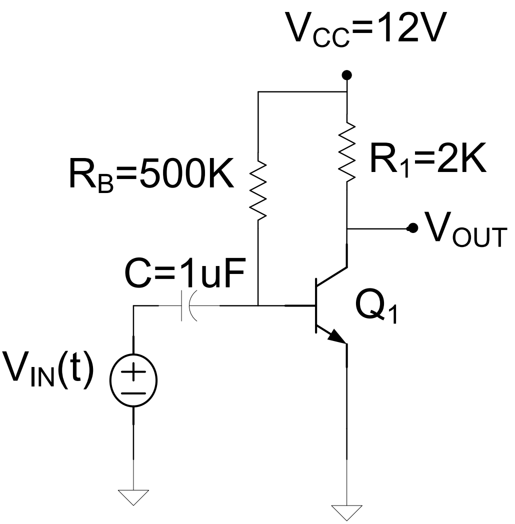


ss equivalent circuit

This basic amplifier structure is widely used and repeated analysis serves no useful purpose

Have seen this circuit before but will repeat for review purposes

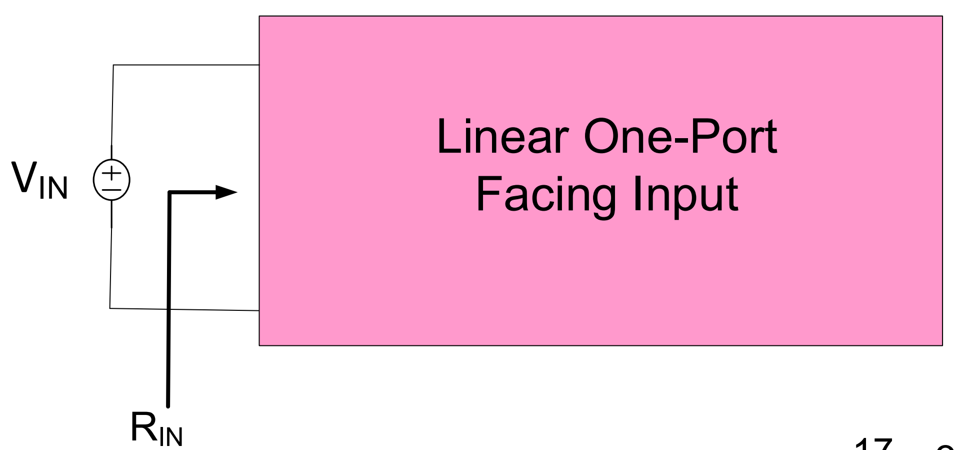
Amplifier Characterization (an example)



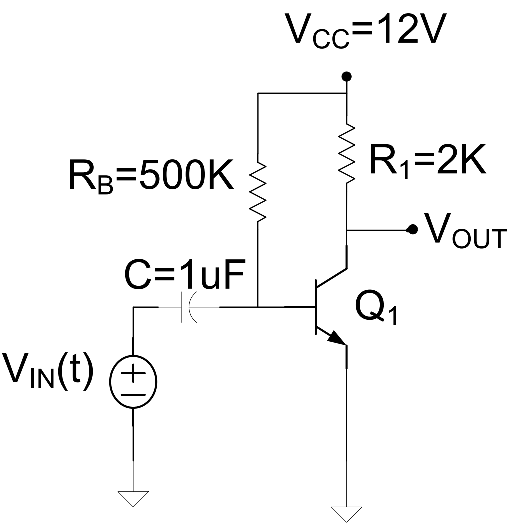
Determine V_{OUTQ}, A_V, R_{IN}

β=100

- Here R_{IN} is defined to be the impedance facing V_{IN}
- Here any load is assumed to be absorbed into the one-port
- Later will consider how load is connected in defining R_{IN}

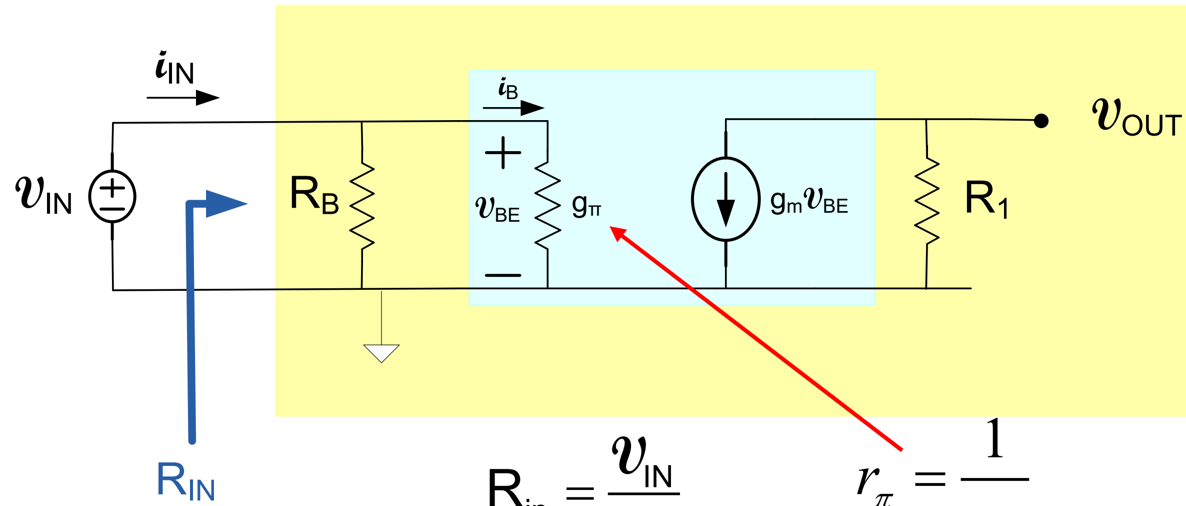


Amplifier Characterization (an example)

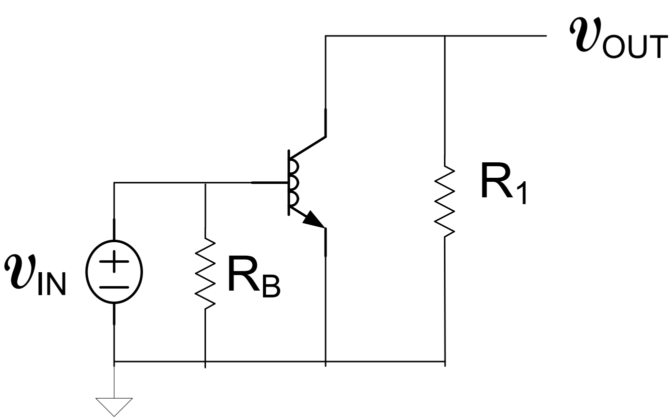


β=100

Determine R_{IN}



$$R_{in} = \frac{v_{IN}}{i_{IN}} \qquad r_\pi = \frac{1}{g_\pi}$$



ss equivalent circuit

$$R_{in} = R_B // r_\pi$$

Usually $R_B >> r_\pi$

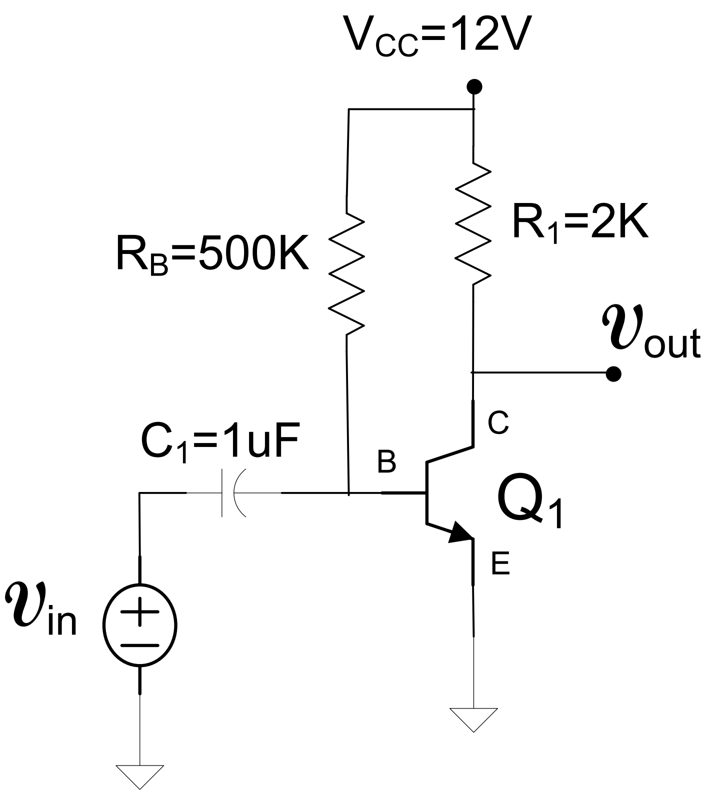
$$R_{in} = R_B // r_\pi \cong r_\pi$$

$$R_{in} \cong r_\pi = \left(\frac{I_{CQ}}{\beta V_t} \right)^{-1}$$

$$R_{in} \cong \left(\frac{2.3\text{mA}}{100 \bullet 25\text{mV}} \right)^{-1} = 1087\Omega$$

Amplifier Characterization (an example)

Determine v_{OUT} and $V_{OUT}(t)$ if v_{IN}=.002sin(400t)



$$v_{OUT} = A_V v_{IN}$$

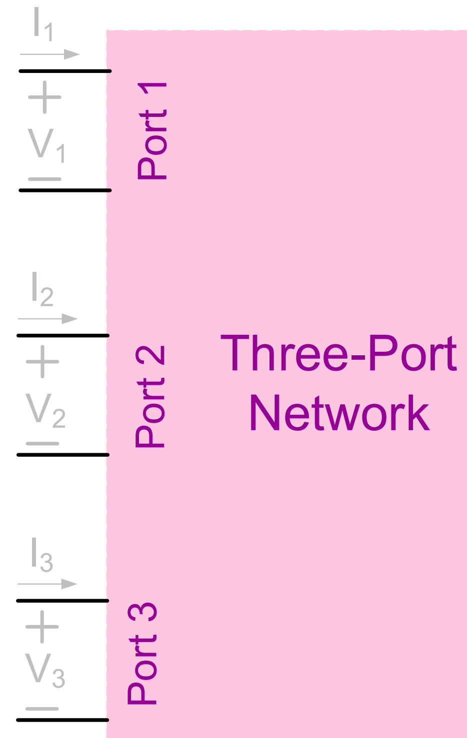
$$v_{OUT} = -177 \bullet .002\sin(400t) = -0.354\sin(400t)$$

$$V_{OUT}(t) \cong V_{OUTQ} + A_V v_{IN}$$

$$V_{OUT} \cong 7.4V - 0.35 \bullet \sin(400t)$$

This example identified several useful characteristics of amplifiers but a more formal method of characterization is needed!

One-Port, Two-Port and Three-Port Networks



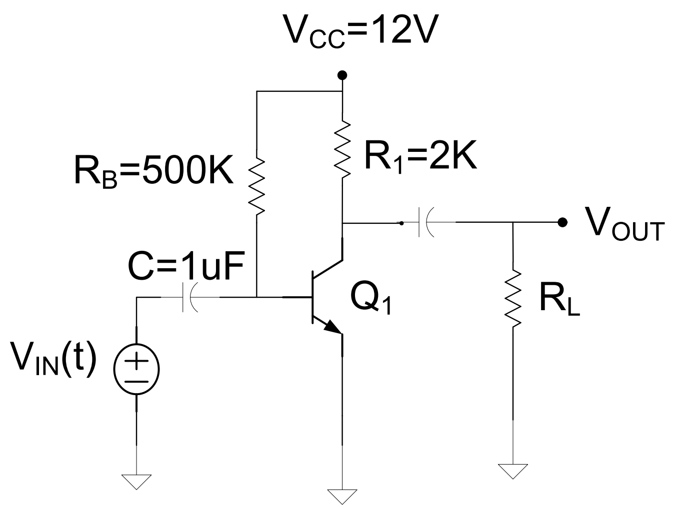
- Each port characterized by a pair of nodes (terminals)
- Can consider any number of ports
- Can be linear or nonlinear but most interest here will be in linear n-ports
- Often one node is common for all ports
- Ports are externally excited, terminated, or interconnected to form useful circuits
- Often useful for decomposing portions of a larger circuit into subcircuits to provide additional insight into operation

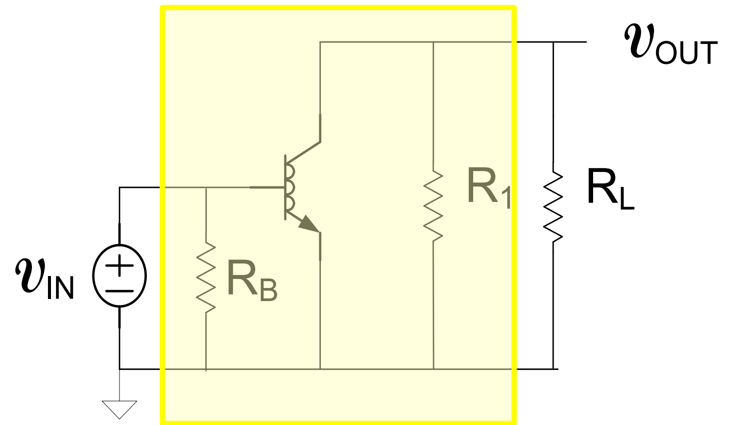
Amplifier Characterization

- Two-Port Models
- Amplifier Parameters

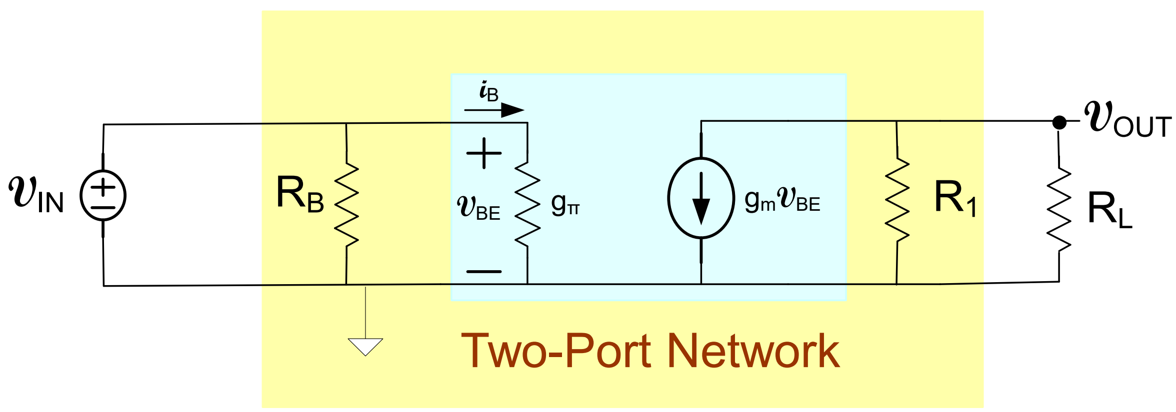
Will assume amplifiers have two ports, one termed an input port and the other termed an output port

Two-Port Representation of Amplifiers





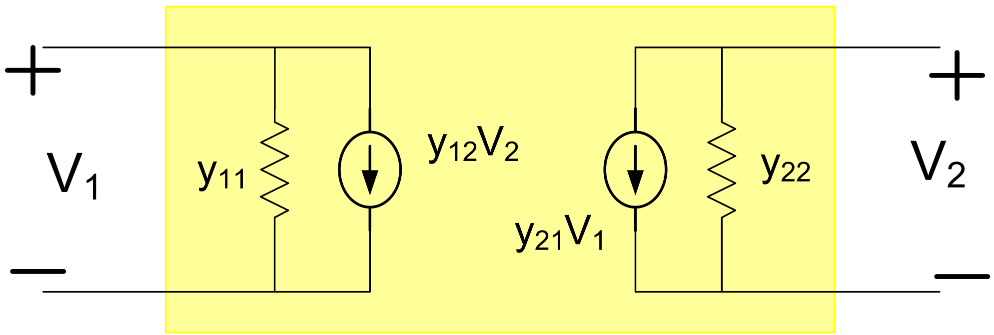
Have excluded R_L from two-port here



- Two-port model representation of amplifiers useful for insight into operation and analysis
- Internal circuit structure of the two-port can be quite complicated but equivalent two-port model (when circuit is linear) is quite simple

Two-port representation of amplifiers

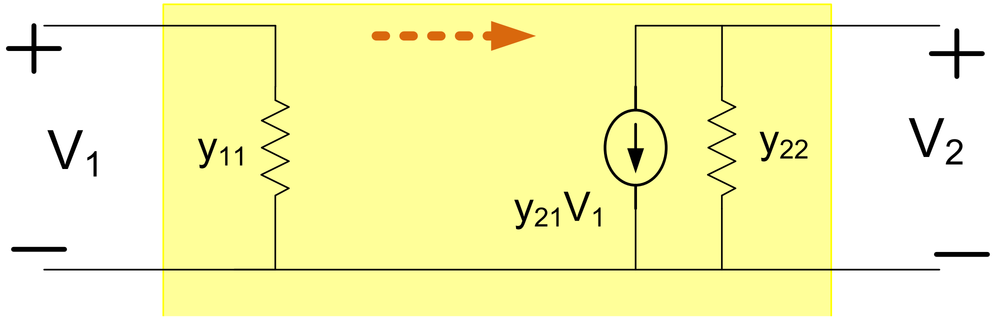
Amplifiers can be modeled as a linear two-port for small-signal operation



In terms of y-parameters

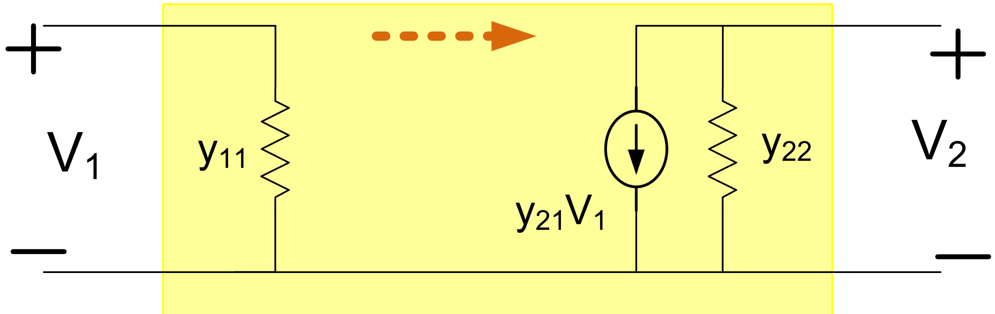
Other parameter sets could be used

- Amplifier often **unilateral** (signal propagates in only one direction: wlog $y_{12}=0$)
- One terminal is often common

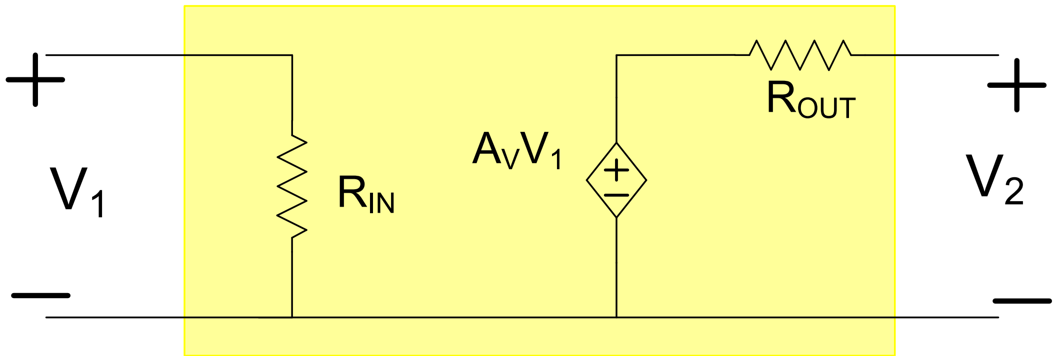


Two-port representation of amplifiers

Unilateral amplifiers:



- Thevenin equivalent output port often more standard
- R_{IN}, A_V, and R_{OUT} often used to characterize the two-port of amplifiers



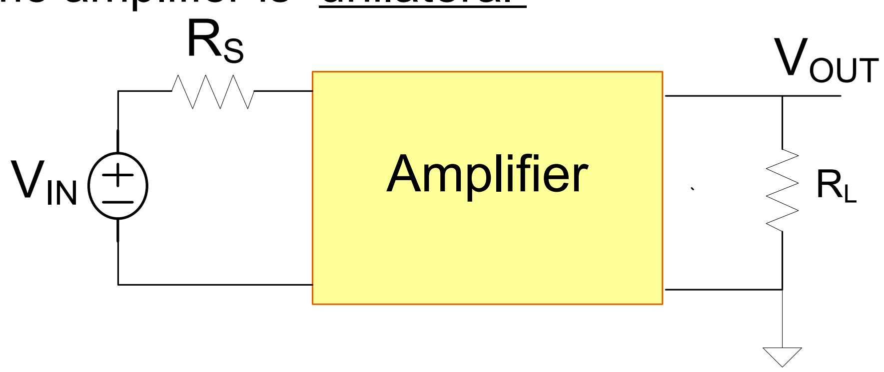
Unilateral amplifier in terms of "amplifier" parameters

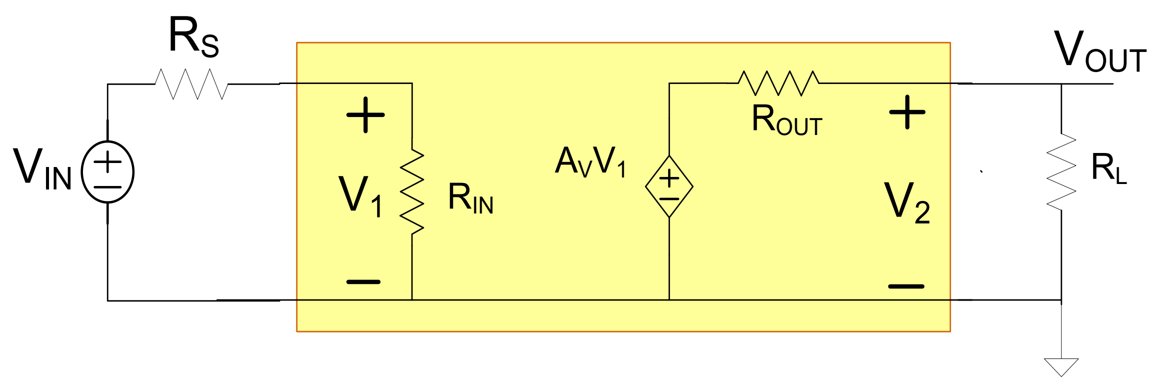
$$R_{IN} = \frac{1}{y_{11}} \qquad A_V = -\frac{y_{21}}{y_{22}} \qquad R_{OUT} = \frac{1}{y_{22}}$$

Amplifier input impedance, output impedance and gain are usually of interest

Why?

Example 1: Assume amplifier is <u>unilateral</u>





$$V_{OUT} = \left(\frac{R_L}{R_L + R_{OUT}}\right) A_V \left(\frac{R_{IN}}{R_S + R_{IN}}\right) V_{IN}$$

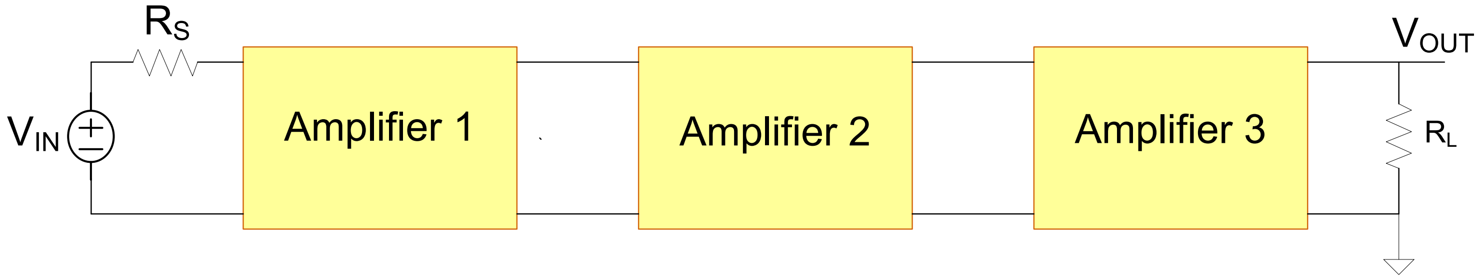
$$A_{VAMP} = \frac{V_{OUT}}{V_{IN}} = \left(\frac{R_L}{R_L + R_{OUT}}\right)\left(\frac{R_{IN}}{R_S + R_{IN}}\right) A_V$$

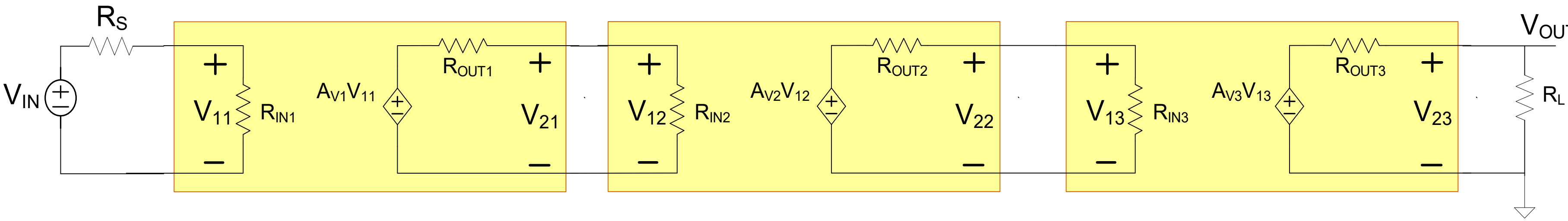
- Can get gain without reconsidering details about components internal to the Amplifier !!!
- Analysis more involved when not unilateral

Amplifier input impedance, output impedance and gain are usually of interest

Why?

Example 2: Assume amplifiers are unilateral





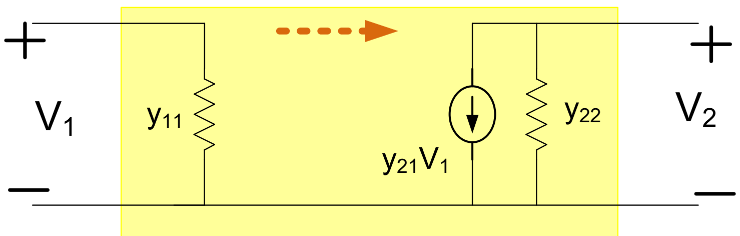
$$V_{OUT}=\left(\frac{R_L}{R_L+R_{OUT3}}\right)A_{V3}\left(\frac{R_{IN3}}{R_{OUT2}+R_{IN3}}\right)A_{V2}\left(\frac{R_{IN2}}{R_{OUT1}+R_{IN2}}\right)A_{V1}\left(\frac{R_{IN1}}{R_S+R_{IN1}}\right)V_{IN}$$

$$A_{VAMP}=\frac{V_{OUT}}{V_{IN}}=\left(\frac{R_L}{R_L+R_{OUT3}}\right)A_{V3}\left(\frac{R_{IN3}}{R_{OUT2}+R_{IN3}}\right)A_{V2}\left(\frac{R_{IN2}}{R_{OUT1}+R_{IN2}}\right)A_{V1}\left(\frac{R_{IN1}}{R_S+R_{IN1}}\right)$$

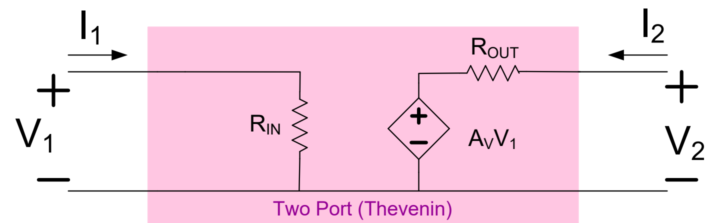
- Can get gain without reconsidering details about components internal to the Amplifier !!!
- Analysis more involved when not unilateral

Two-port representation of amplifiers

- Amplifier often **unilateral** (signal propagates in only one direction: wlog $y_{12}=0$)
- One terminal is often common
- "Amplifier" parameters often used

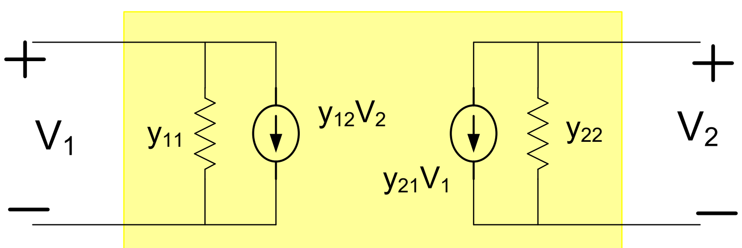


y parameters

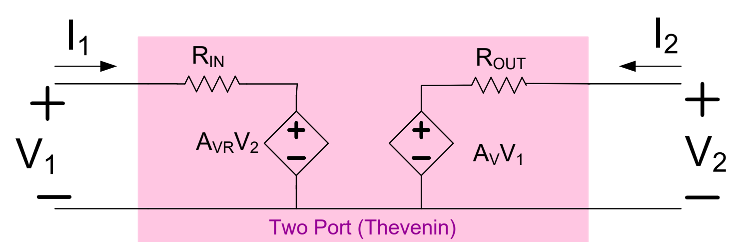


Amplifier parameters

- Amplifier parameters can also be used if not **unilateral**
- One terminal is often common

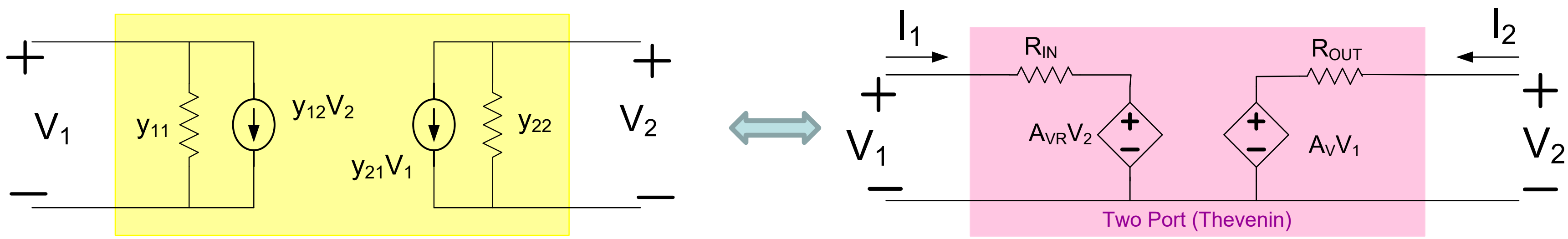


y parameters



Amplifier parameters

Determination of small-signal model parameters:



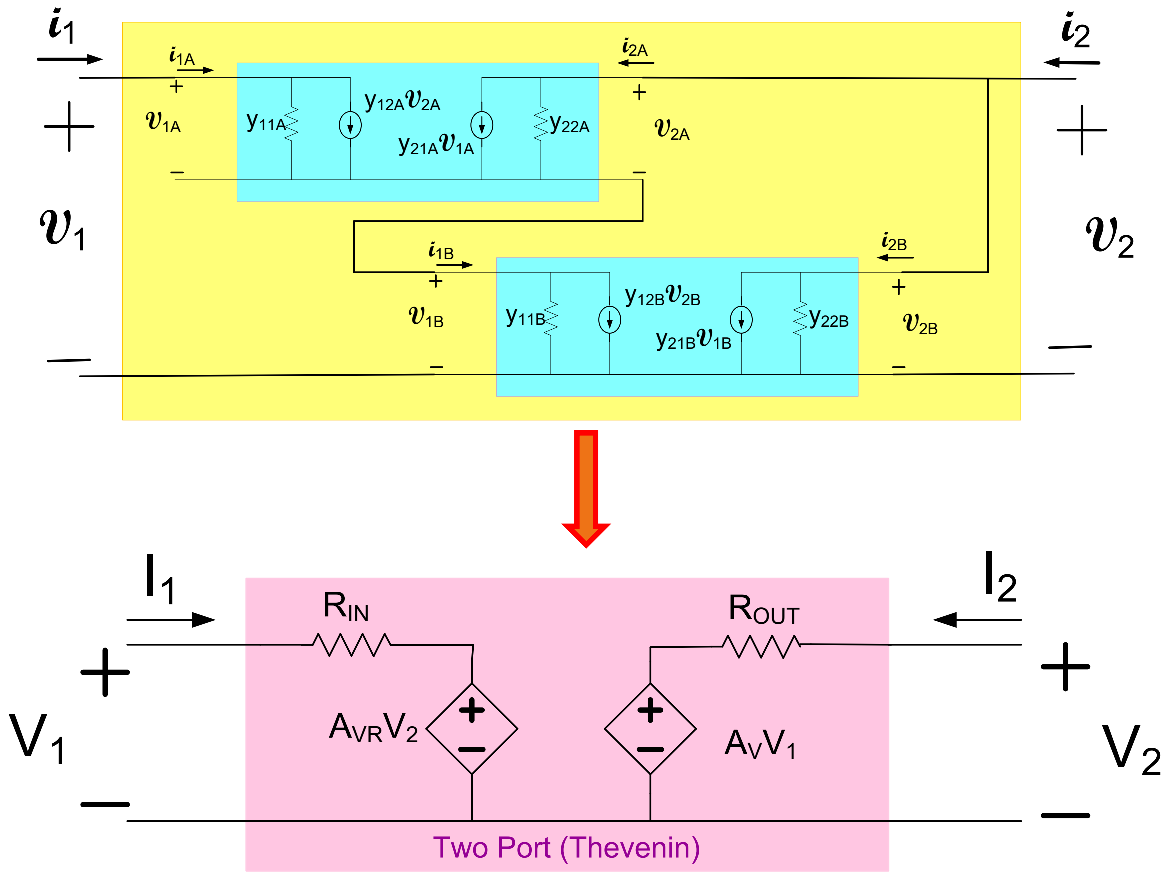
In the past, we have determined small-signal model parameters of electronic devices from the nonlinear port characteristics

$$\left.\begin{aligned} \mathbf{I_1} &= \mathbf{f_1}(\mathbf{V_1},\mathbf{V_2}) \\ \mathbf{I_2} &= \mathbf{f_2}(\mathbf{V_1},\mathbf{V_2}) \end{aligned}\right\} \qquad \mathbf{y_{ij}} = \left.\frac{\partial \mathbf{f_i}(\mathbf{V_1},\mathbf{V_2})}{\partial \mathbf{V_j}}\right|_{\vec{\mathbf{V}}=\vec{\mathbf{V}}_\mathbf{Q}}$$

- Will now determine small-signal model parameters for two-port comprised of linear networks (instead of just electronic devices)
- Could go back to the nonlinear models and analyze as we did for electronic devices
- Will follow a different approach (results are identical) that is often much easier

Two-Port Equivalents of Interconnected Two-ports

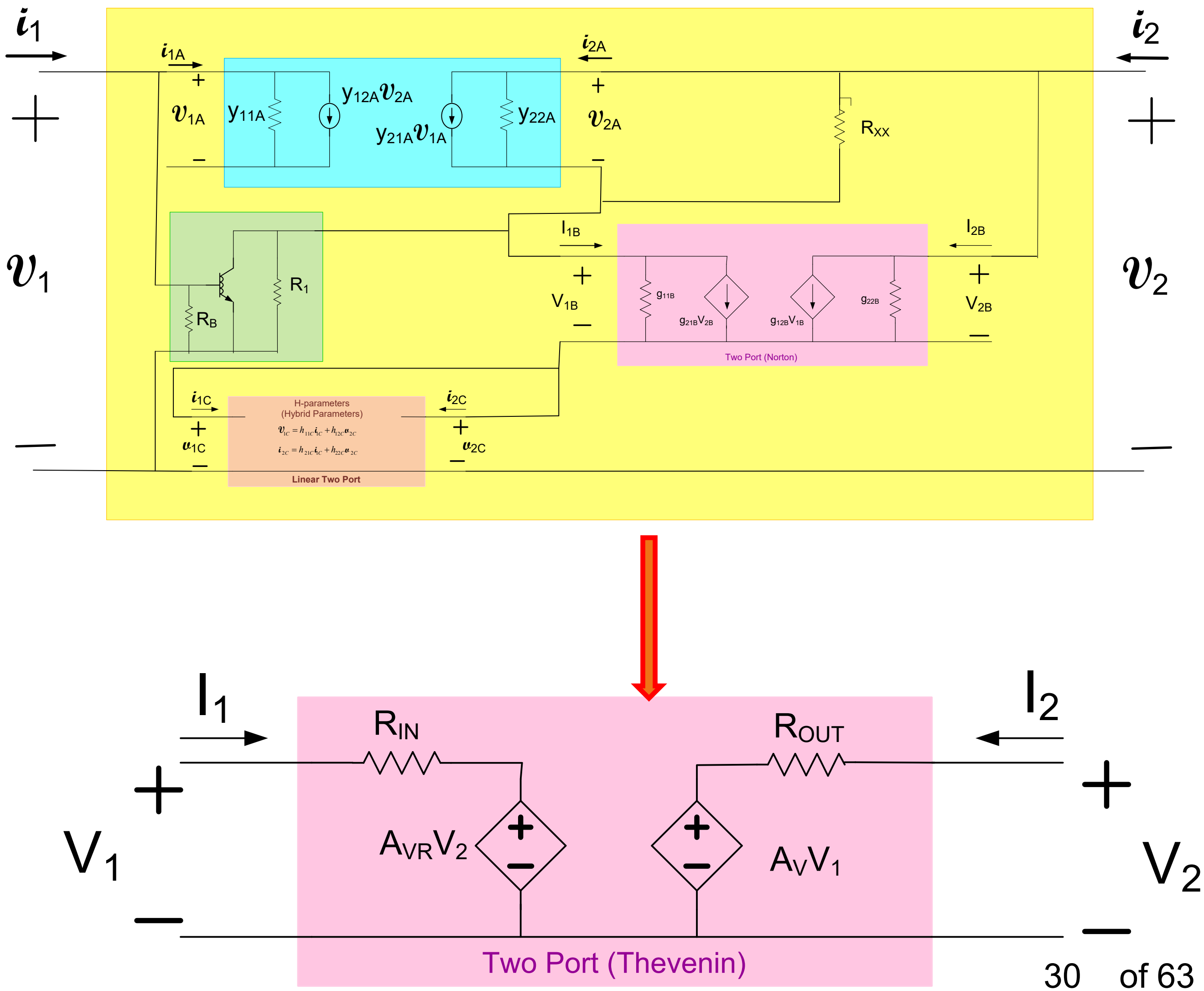
Example:



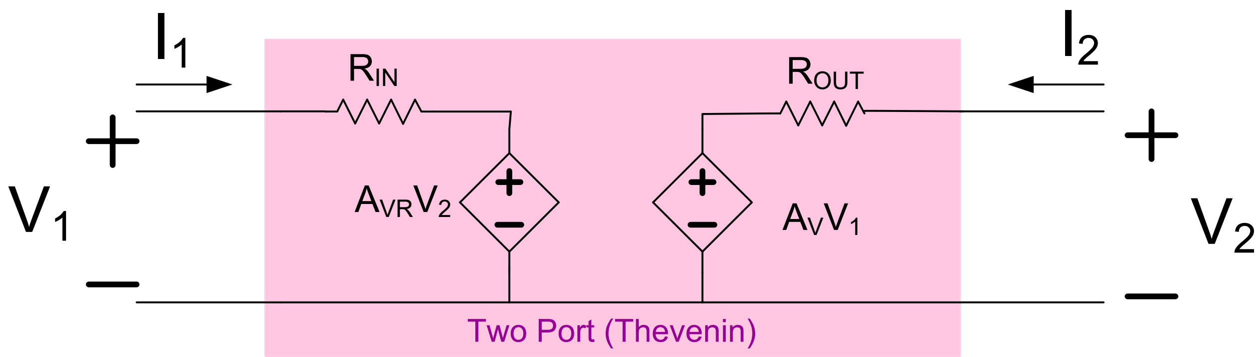
- could obtain two-port in any form
- often obtain equivalent circuit w/o identifying independent variables
- Unilateral iff $A_{VR}=0$ (or if $A_V=0$ though would probably relabel ports)
- Thevenin-Norton transformations can be made on either or both ports

Two-Port Equivalents of Interconnected Two-ports

Example:



Two-Port Equivalents of Interconnected Two-ports



$$v_1 = i_1 R_{in} + A_{VR} v_2$$

$$v_2 = i_2 R_0 + A_{V0} v_1$$

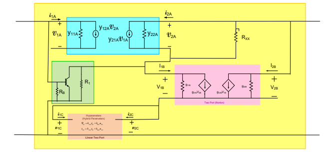
Or equivalently in form where port voltages are the independent variables

$$i_1 = v_1\left(\frac{1}{R_{in}}\right) + v_2\left(\frac{-A_{VR}}{R_{in}}\right)$$

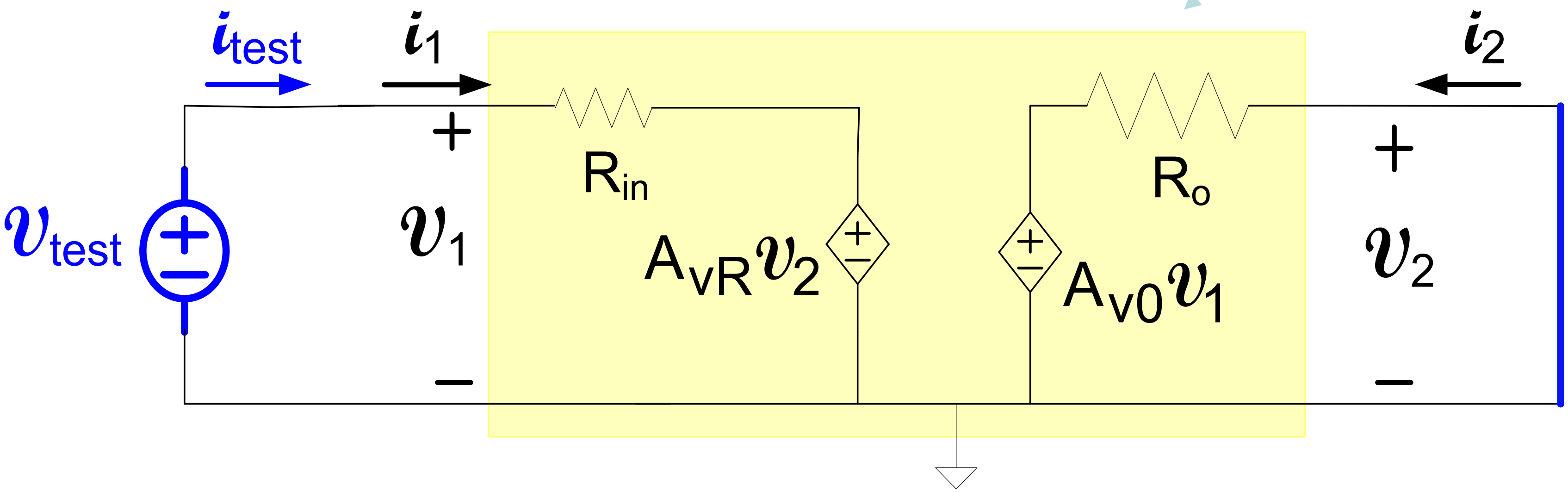
$$i_2 = v_1\left(\frac{-A_{V0}}{R_0}\right) + v_2\left(\frac{1}{R_0}\right)$$

Determination of two-port small-signal model parameters

(One method will be discussed here)



A method of obtaining R_{in}



Terminate the output in a (small signal) short-circuit

$$\left.\begin{aligned} i_1 &= v_1\left(\frac{1}{R_{in}}\right) + v_2\left(\frac{-A_{VR}}{R_{in}}\right)\\ i_2 &= v_1\left(\frac{-A_{V0}}{R_0}\right) + v_2\left(\frac{1}{R_0}\right)\end{aligned}\right\}$$

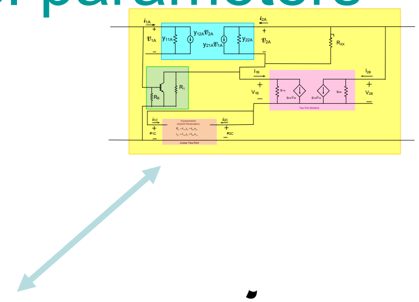
$$\xrightarrow{v_2 = 0}$$

$v_1 = v_{test}$

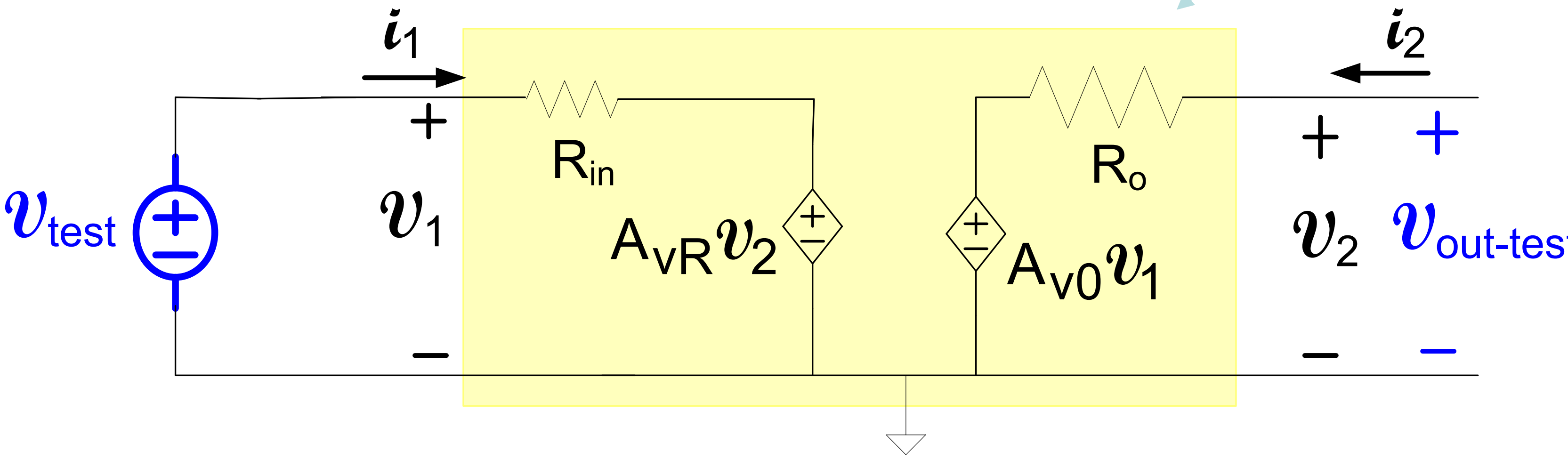
$i_1 = i_{test}$

$$R_{in} = \frac{v_{test}}{i_{test}}$$

Determination of two-port small-signal model parameters



A method of obtaining A_{V0}

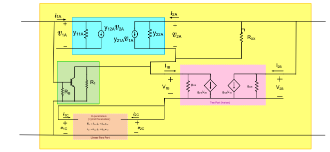


Terminate the output in a (small signal) open-circuit

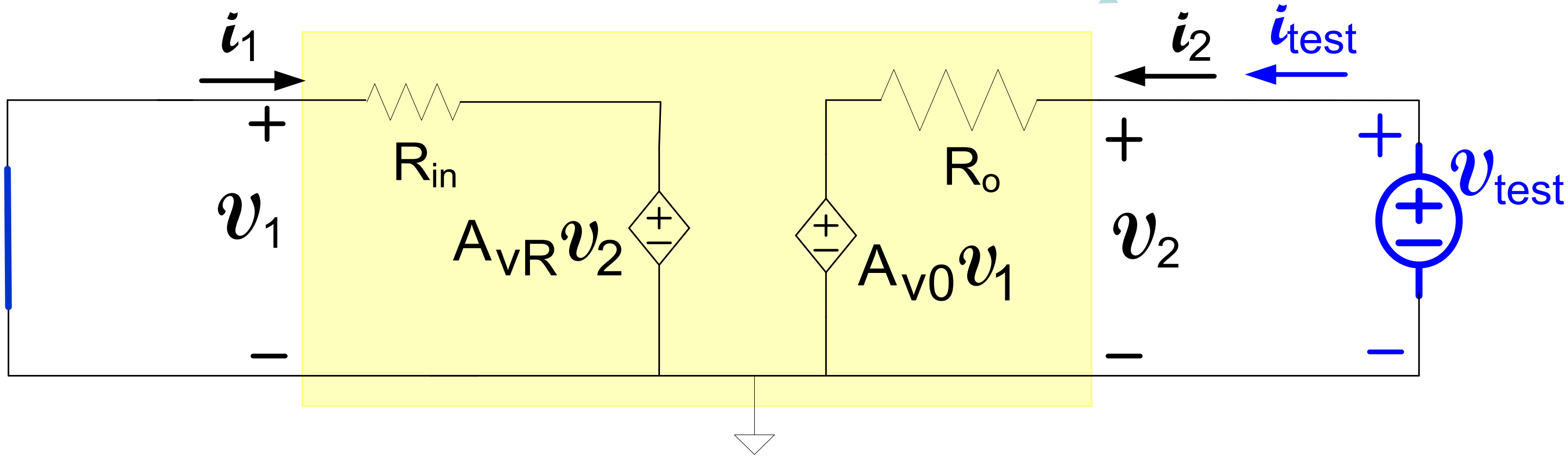
$$\left.\begin{aligned} i_1 &= v_1\left(\frac{1}{R_{in}}\right) + v_2\left(\frac{-A_{VR}}{R_{in}}\right) \\ i_2 &= v_1\left(\frac{-A_{V0}}{R_0}\right) + v_2\left(\frac{1}{R_0}\right) \end{aligned}\right\} \xrightarrow{i_2 = 0} \begin{aligned} v_1 &= v_{\text{test}} \\ v_2 &= v_{\text{out-test}} \end{aligned}$$

$$A_{V0} = \frac{v_{\text{out-test}}}{v_{\text{test}}}$$

Determination of two-port small-signal model parameters



A method of obtaining R_0

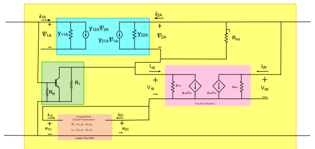


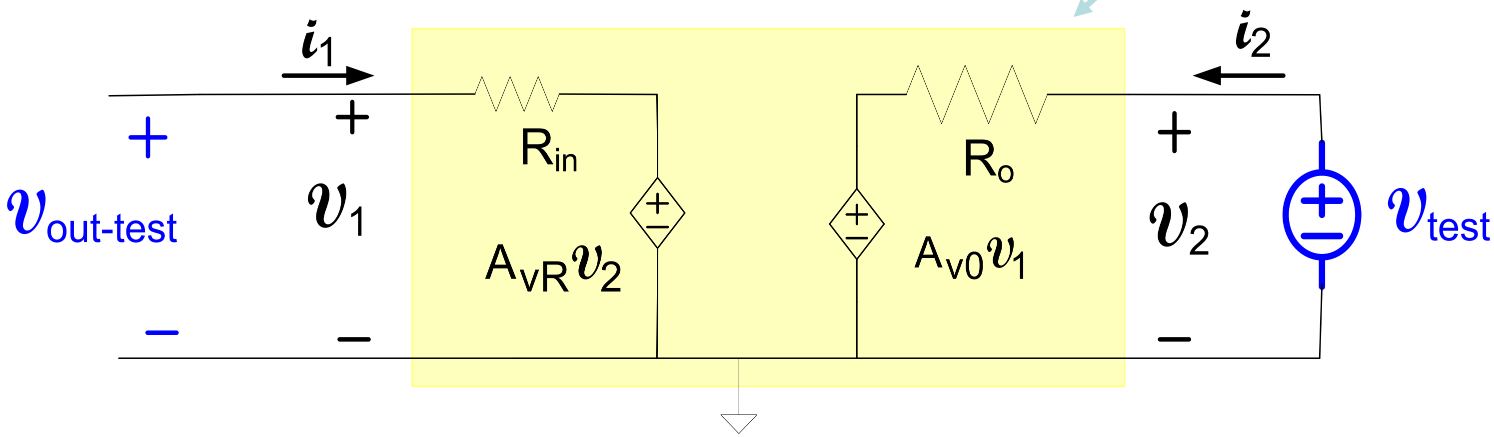
Terminate the input in a (small-signal) short-circuit

$$\left.\begin{aligned} i_1 &= v_1\left(\frac{1}{R_{in}}\right) + v_2\left(\frac{-A_{VR}}{R_{in}}\right) \\ i_2 &= v_1\left(\frac{-A_{V0}}{R_0}\right) + v_2\left(\frac{1}{R_0}\right) \end{aligned}\right\} \xrightarrow{v_1 = 0} \quad R_0 = \frac{v_{test}}{i_{test}}$$

Determination of two-port small-signal model parameters

A method of obtaining A_{VR}





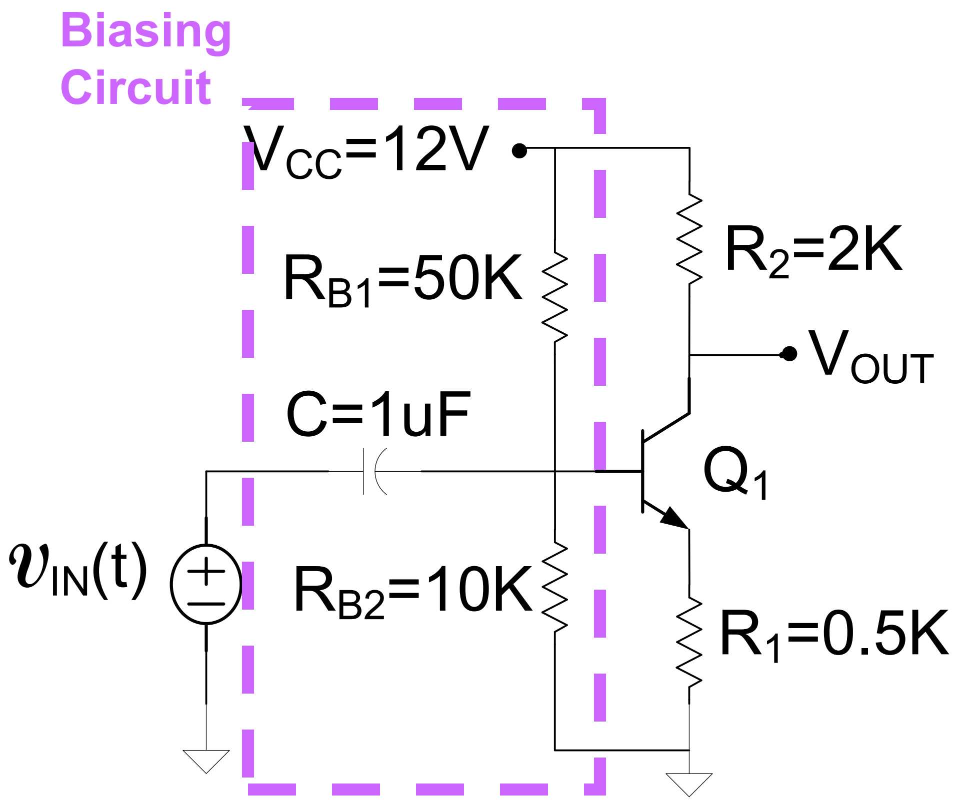
Terminate the <u>input</u> in a (small-signal) open-circuit

$$\left.\begin{aligned} i_1 &= v_1\left(\frac{1}{R_{in}}\right) - v_2\left(\frac{A_{VR}}{R_{in}}\right) \\ i_2 &= v_1\left(\frac{-A_{V0}}{R_0}\right) + v_2\left(\frac{1}{R_0}\right) \end{aligned}\right\} \xrightarrow{i_1 = 0} A_{VR} = \frac{v_{out\text{-}test}}{v_{test}}$$

Determination of Amplifier Two-Port Parameters

- Input and output parameters are obtained in exactly the same way, only distinction is in the notation used for the ports.
- Methods given for obtaining amplifier parameters R_{in}, R_{OUT} and A_V for unilateral networks are a special case of the non-unilateral analysis by observing that A_{VR}=0.
- In some cases, other methods for obtaining the amplifier parameters are easier than the "V_{TEST} : I_{TEST}" method that was just discussed

Examples

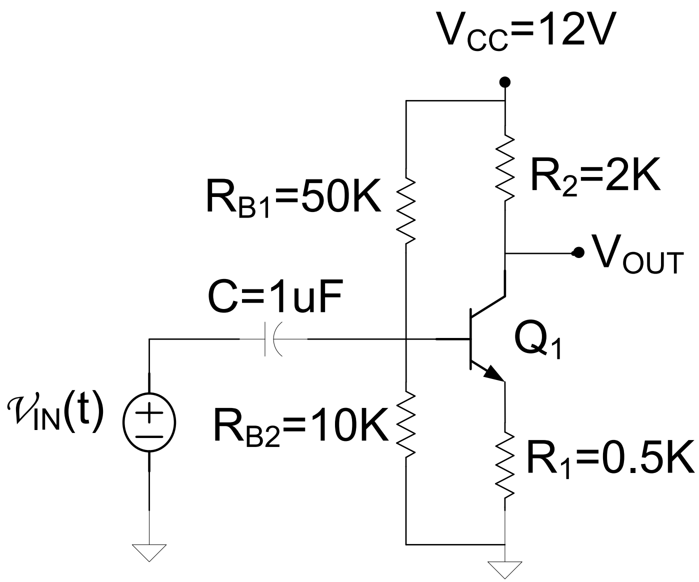


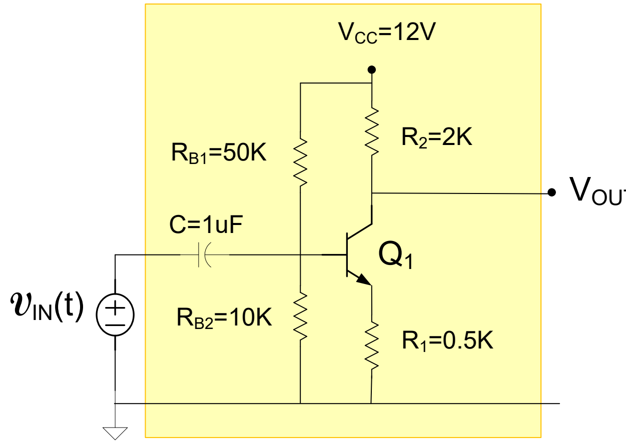
Determine V_{OUTQ} and the SS voltage gain (A_V), assume β=100

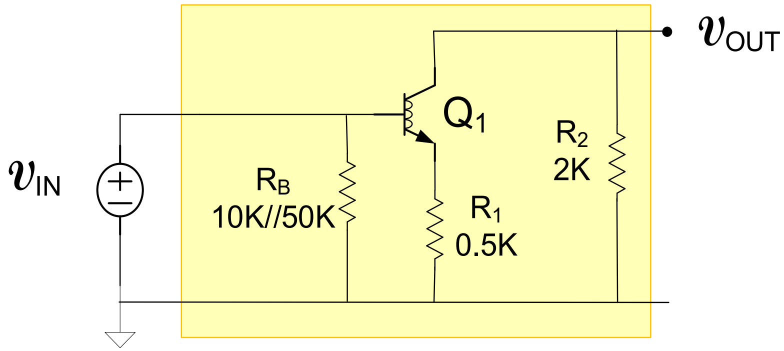
This is a fundamentally different circuit than what we have considered previously !

(A_V is one of the small-signal model parameters for this circuit if treated as two-port with load absorbed into two-port)

Examples



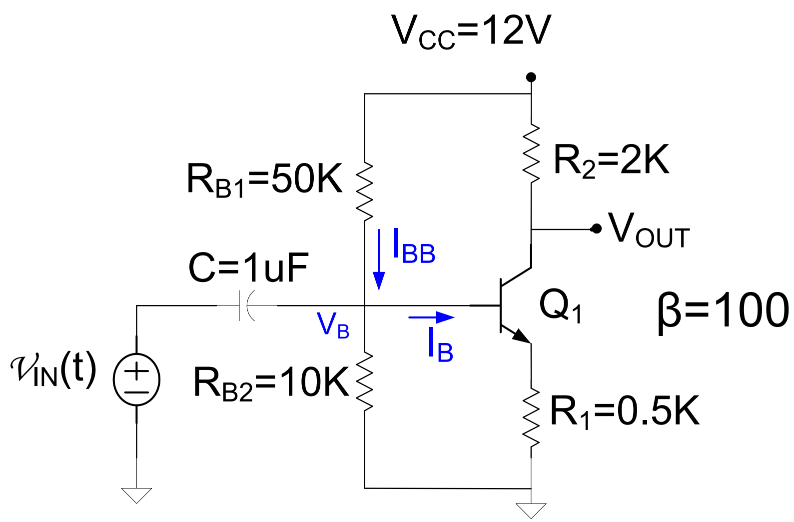


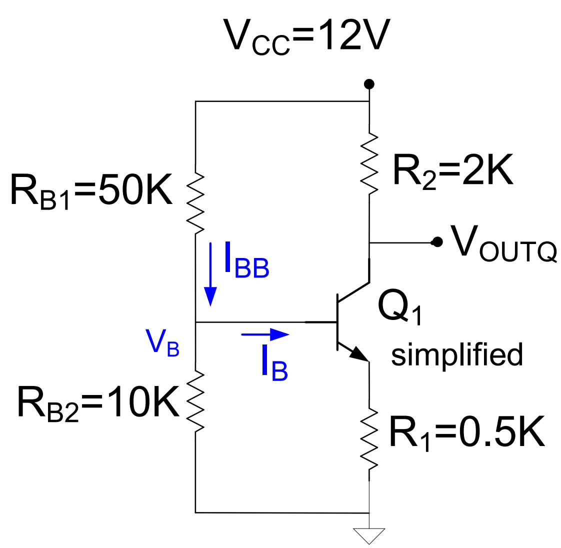


Determine V_{OUTQ} and the SS voltage gain (A_V), assume β=100

(A_V is one of the small-signal model parameters for this circuit)

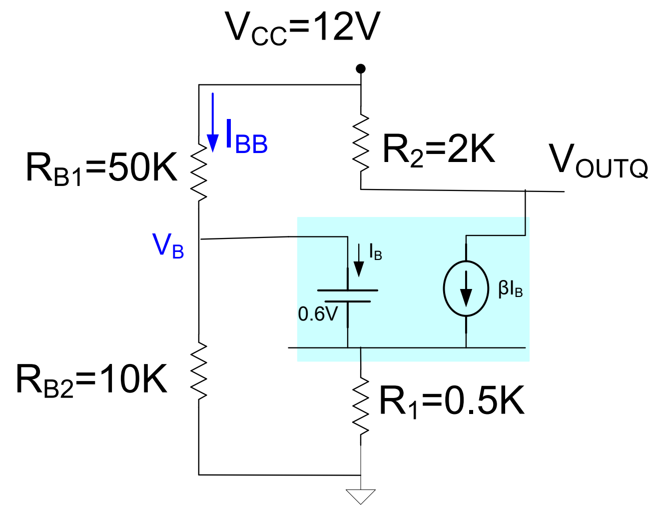
Examples





dc equivalent circuit

Determine V_{OUTQ}



dc equivalent circuit

This circuit is most practical when $I_B \ll I_{BB}$

With this assumption,

$$V_B = \left(\frac{R_{B2}}{R_{B1}+R_{B2}}\right)12V = 2V$$

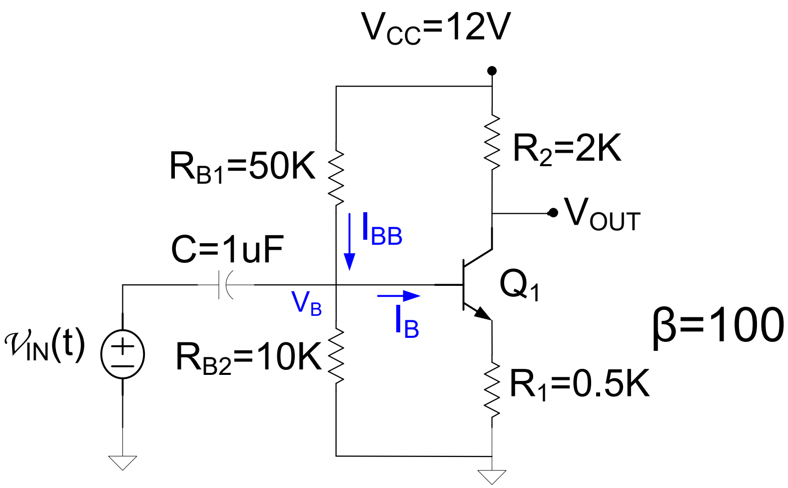
$$I_{CQ} = I_{EQ} = \left(\frac{V_B - 0.6V}{R_1}\right) = \frac{1.4V}{.5K} = 2.8mA$$

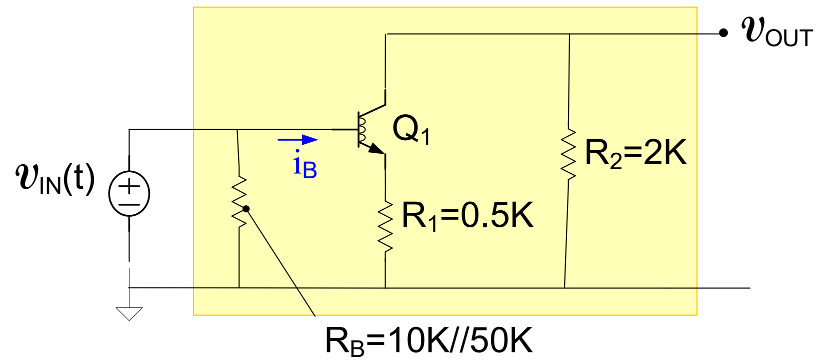
$$V_{OUTQ} = 12V - I_{CQ}R_1 = 6.4V$$

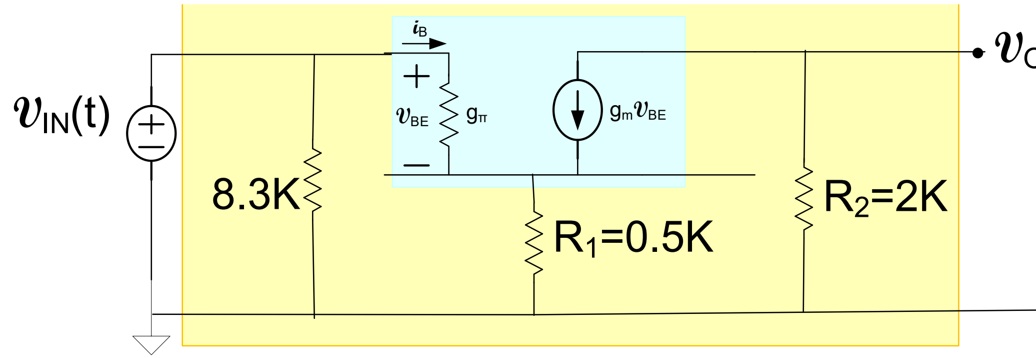
Note: This Q-point is nearly independent of the characteristics of the nonlinear BJT !

Examples

Determine SS voltage gain







$$v_{OUT} = -g_m v_{BE} R_2$$

$$v_{IN} = v_{BE} + R_1\left(v_{BE}\left[g_\pi + g_m\right]\right)$$

$$A_V = \frac{-R_2 g_m v_{BE}}{v_{BE} + R_1\left(v_{BE}\left[g_\pi + g_m\right]\right)} = \frac{-R_2 g_m}{1 + R_1\left(\left[g_\pi + g_m\right]\right)}$$

This voltage gain is nearly independent of the characteristics of the nonlinear BJT !

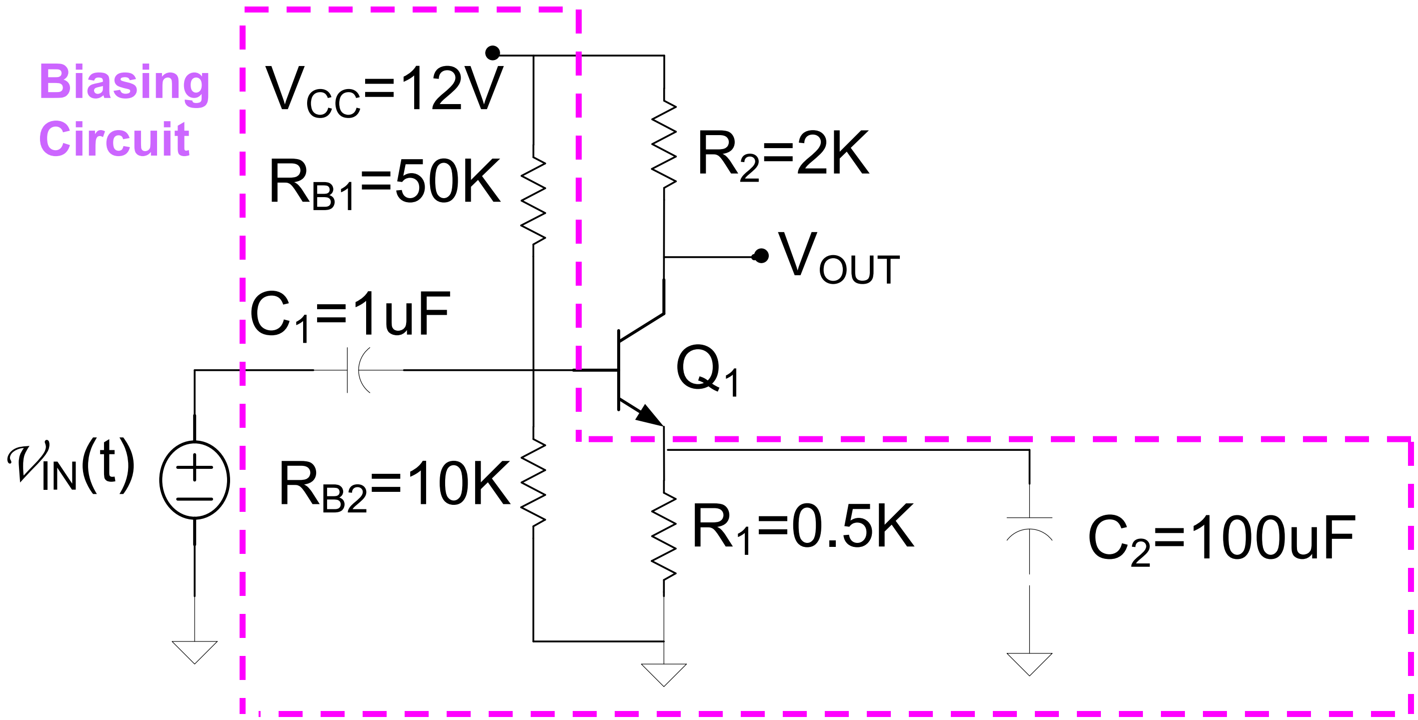
This is a fundamentally different amplifier structure

It can be shown that this is slightly non-unilateral

$g_m R_1$ typically >>1

$$A_V \cong \frac{-R_2 g_m}{R_1 g_m} = \frac{-R_2}{R_1} = -4$$

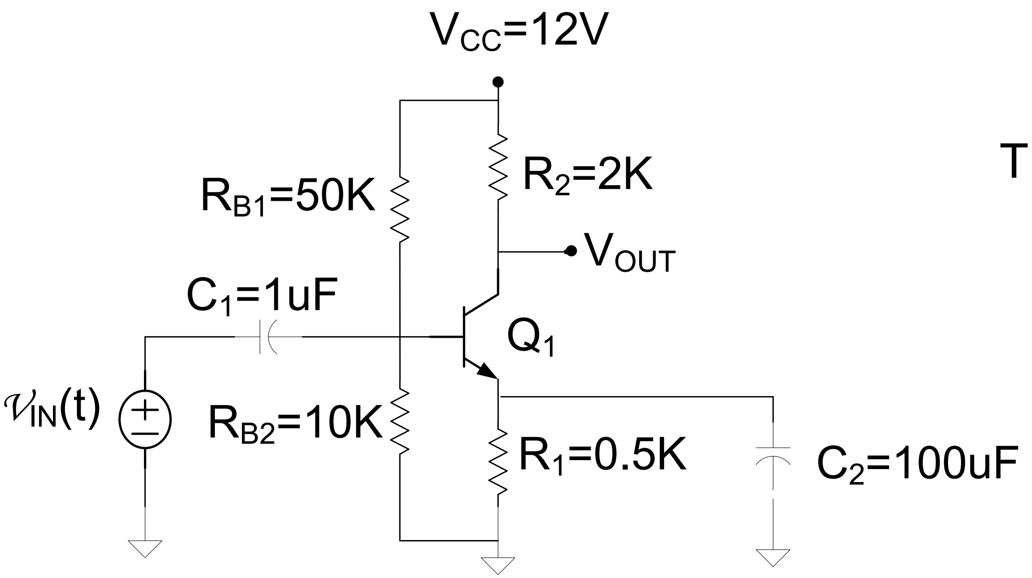
Examples



Determine V_{OUTQ} , R_{IN}, R_{OUT},and the SS voltage gain, and A_{VR} assume β=100

Examples

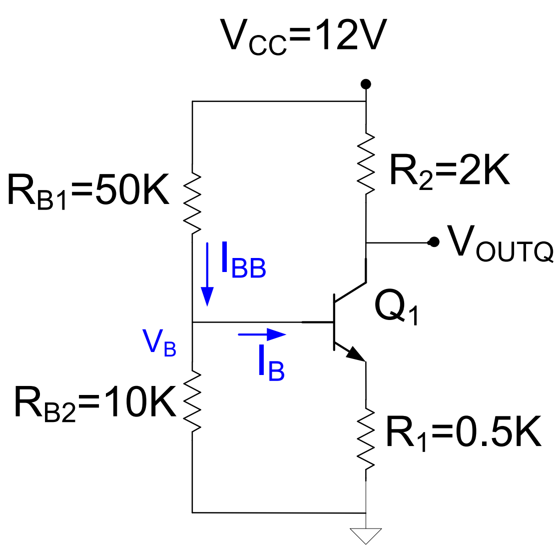
Determine V_{OUTQ}



This is the same as the previous circuit !

$$V_{OUTQ} = 6.4V$$

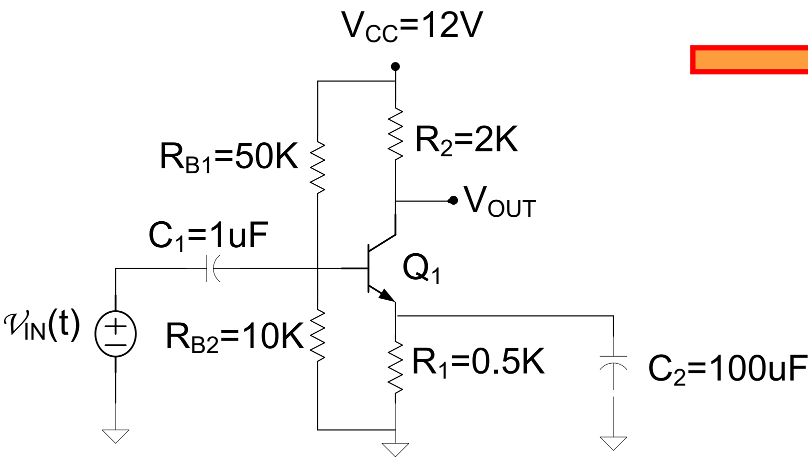
$$I_{CQ} = \frac{5.6V}{2K} = 2.8mA$$

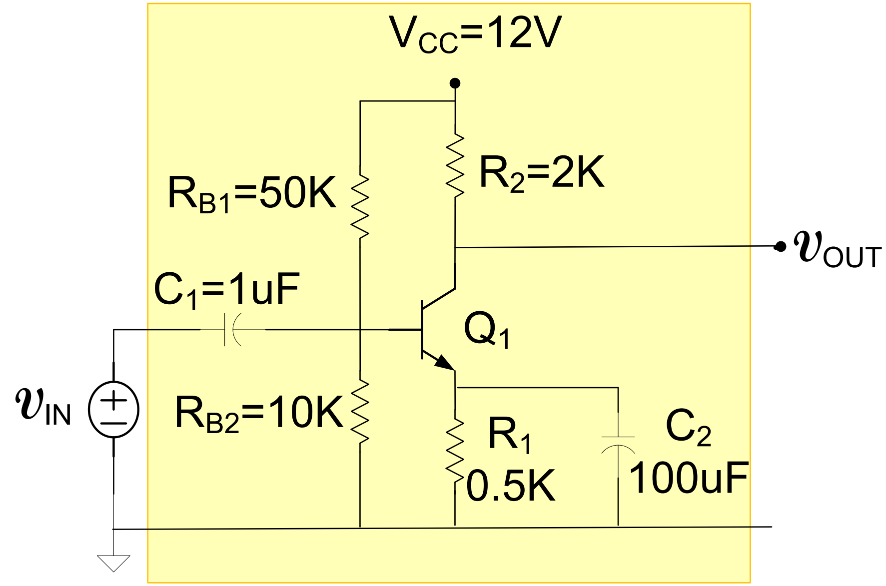


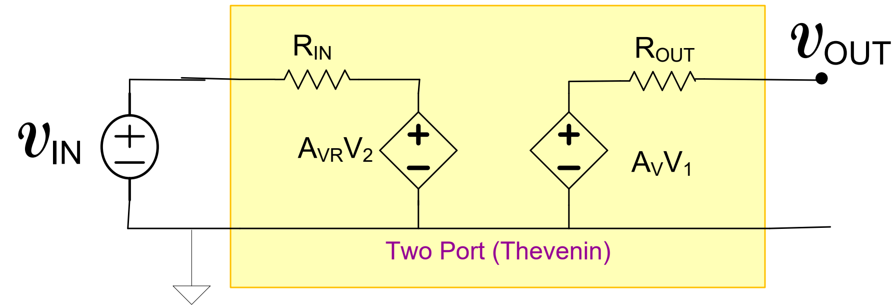
The dc equivalent circuit

Note: This Q-point is nearly independent of the characteristics of the nonlinear BJT !

Examples





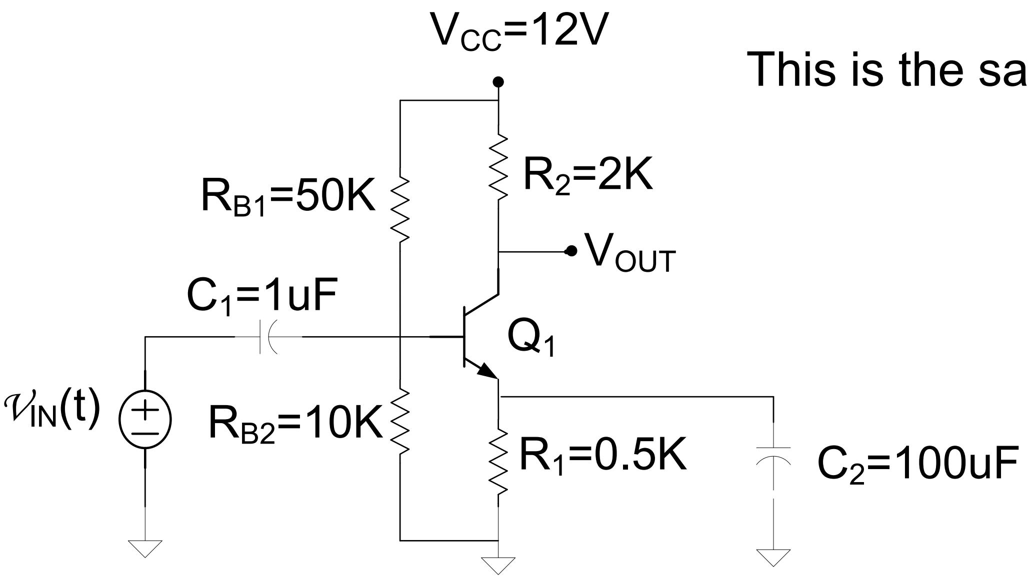


Determine V_{OUTQ} , R_{IN}, R_{OUT}, A_V, and A_{VR}; assume β=100

(A_V , R_{IN}, R_{OUT} , and A_{VR} are the small-signal model parameters for this circuit)

Examples

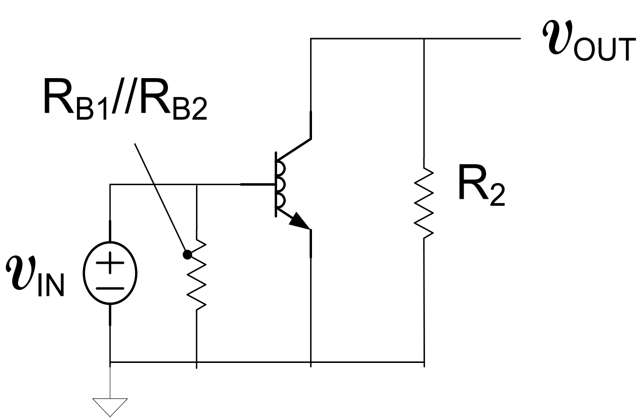
Determine the SS voltage gain A_V



This is the same as another previous-previous circuit !

$$A_V \cong -g_m R_2$$

$$A_V \cong -\frac{I_{CQ} R_2}{V_t}$$



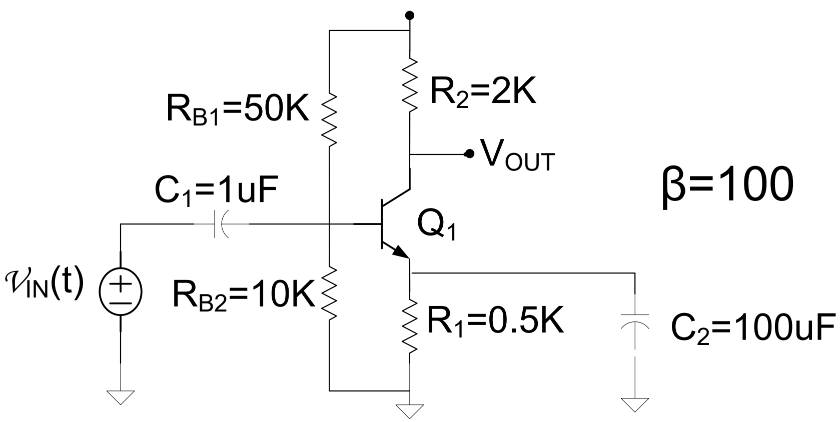
The SS equivalent circuit

$$A_V \cong -\frac{5.6\text{V}}{26\text{mV}} = -215$$

Note: This Gain is nearly independent of the characteristics of the nonlinear BJT !

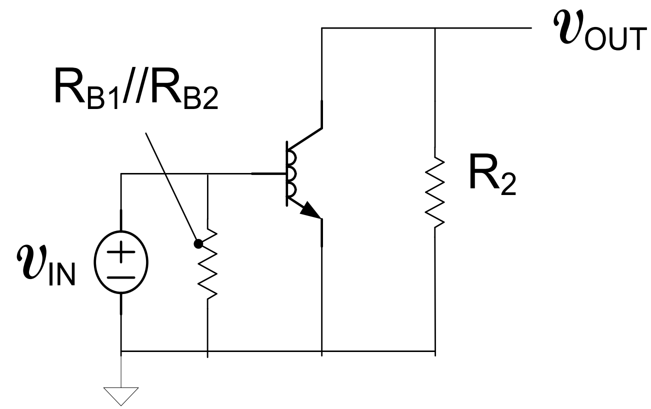
Examples

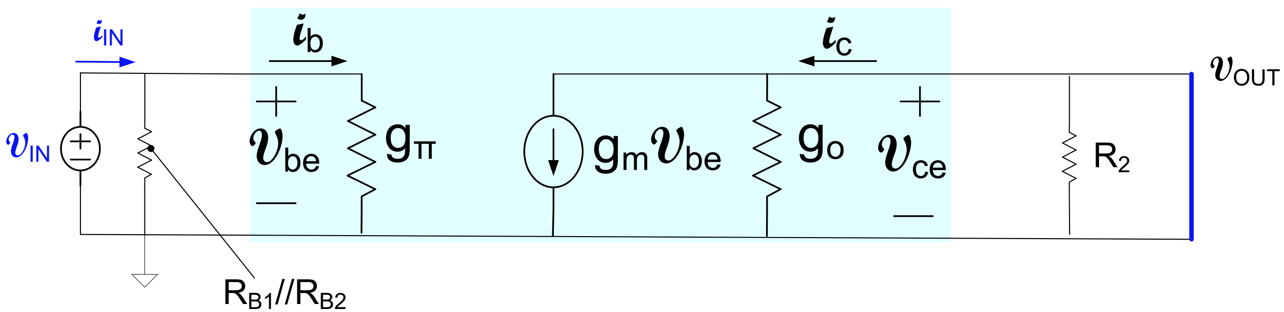
Determination of R_{IN}



$\beta=100$

The SS equivalent circuit





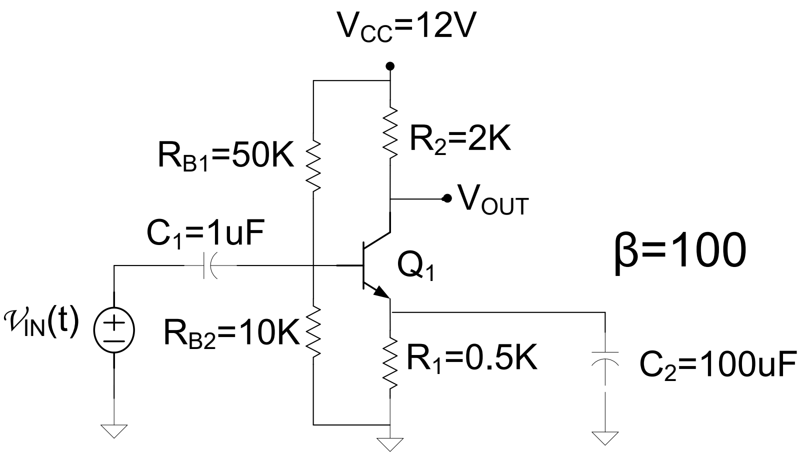
$$R_{IN} = R_{B1}//R_{B2}//r_\pi \cong r_\pi$$

$$r_\pi = \left(\frac{I_{CQ}}{\beta V_t}\right)^{-1} = \left(\frac{2.8mA}{100 \bullet 26mV}\right)^{-1} = 928\Omega$$

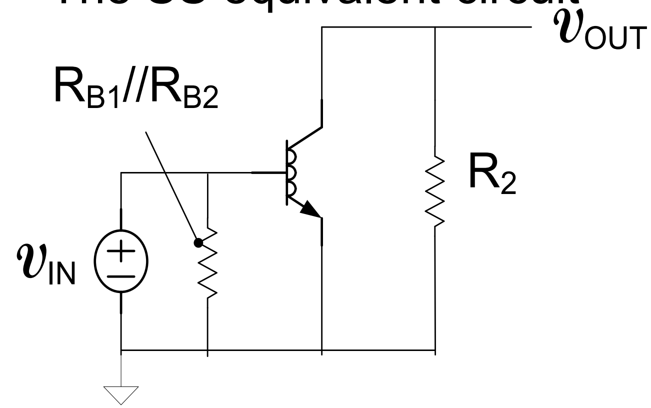
$$R_{IN} = R_{B1}//R_{B2}//r_\pi \cong r_\pi = 930\Omega$$

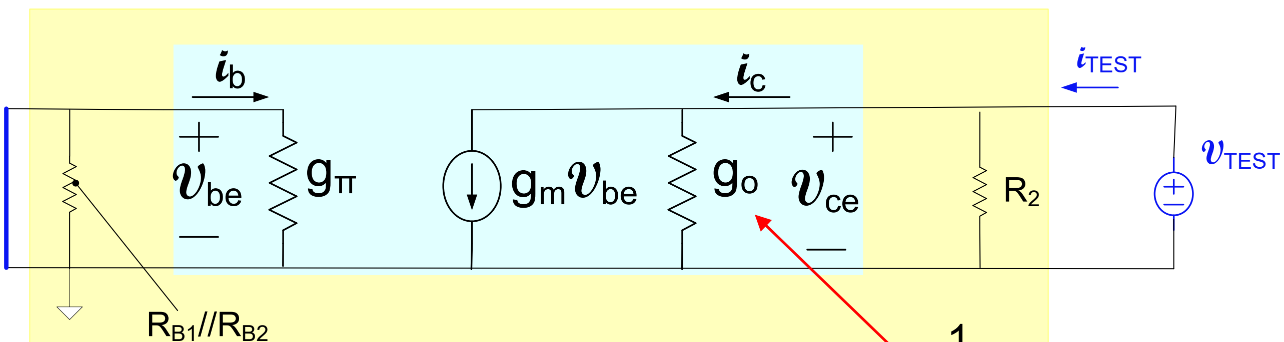
Examples

Determination of R_{OUT}



The SS equivalent circuit





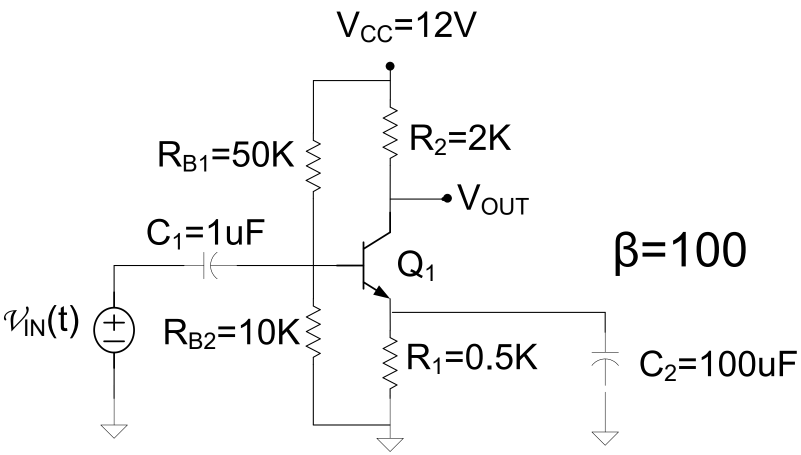
$$r_0 = \frac{1}{g_0}$$

$$R_{OUT} = \frac{v_{TEST}}{i_{TEST}} = R_2 // r_o$$

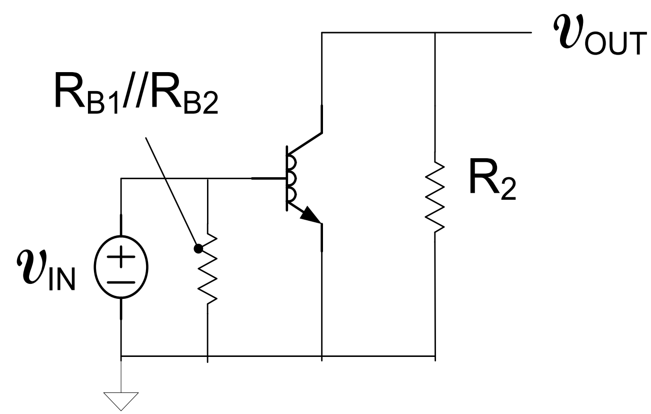
$$r_o = \left(\frac{I_{CQ}}{V_{AF}}\right)^{-1} = \left(\frac{2.8\text{mA}}{200\text{V}}\right)^{-1} = (1.4\text{E-}5)^{-1} = 71\text{K}\Omega$$

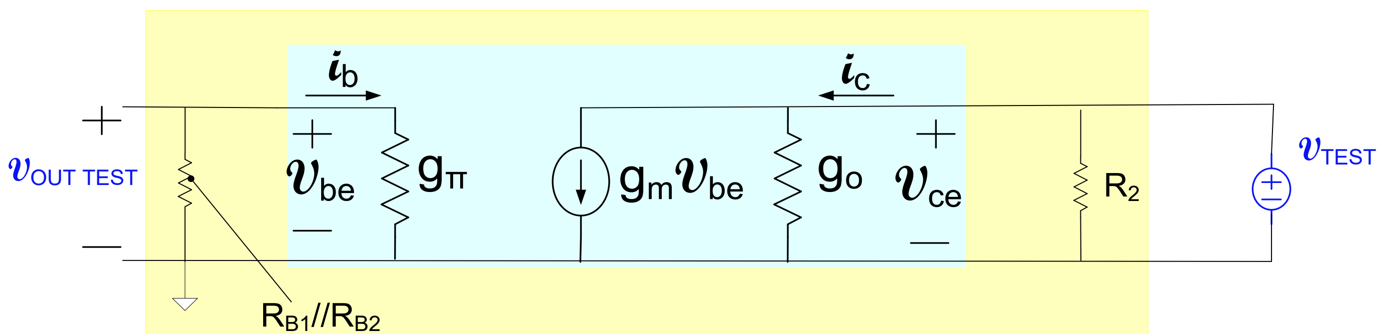
$$R_{OUT} = R_2 // r_o \cong R_2 = 2K$$

Examples   Determine A_{VR}



The SS equivalent circuit



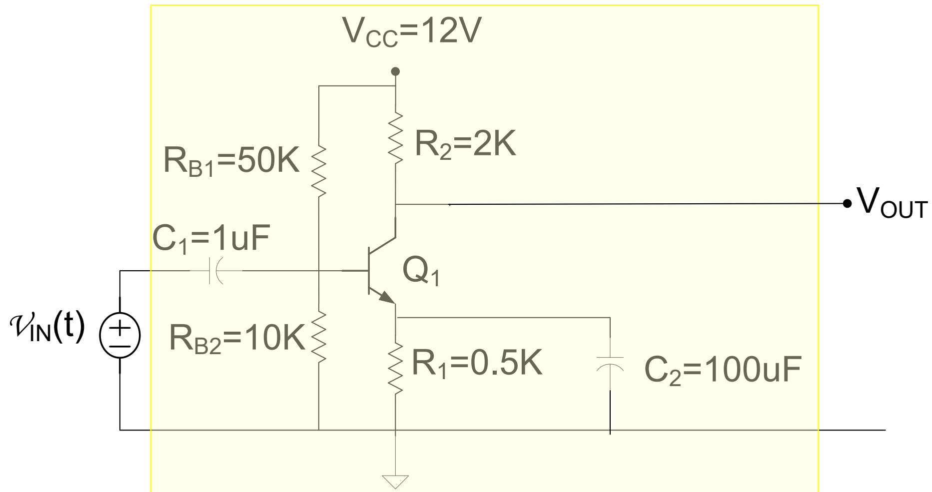


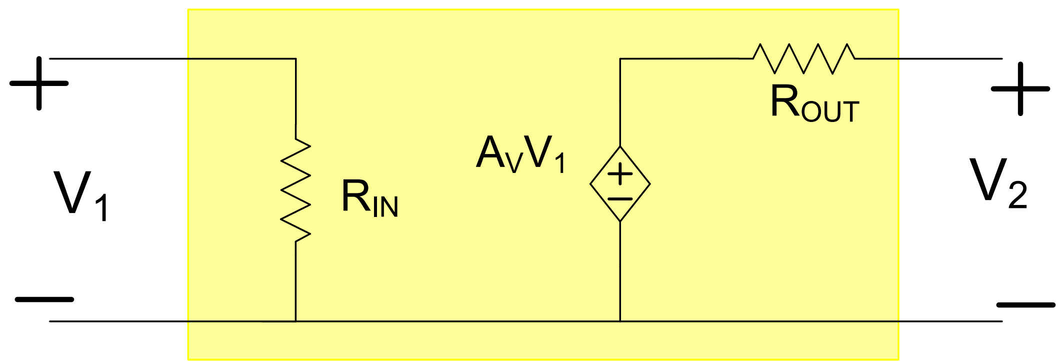
$$v_{OUT\ TEST} = 0$$

$$A_{VR} = 0$$

This circuit is unilateral !

Determination of small-signal two-port representation

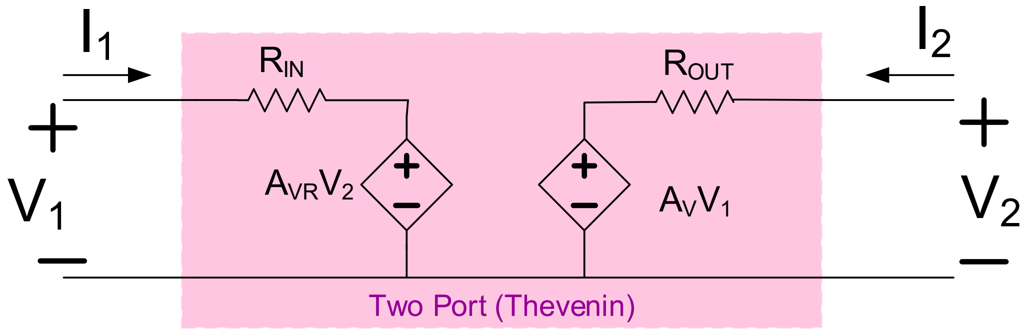




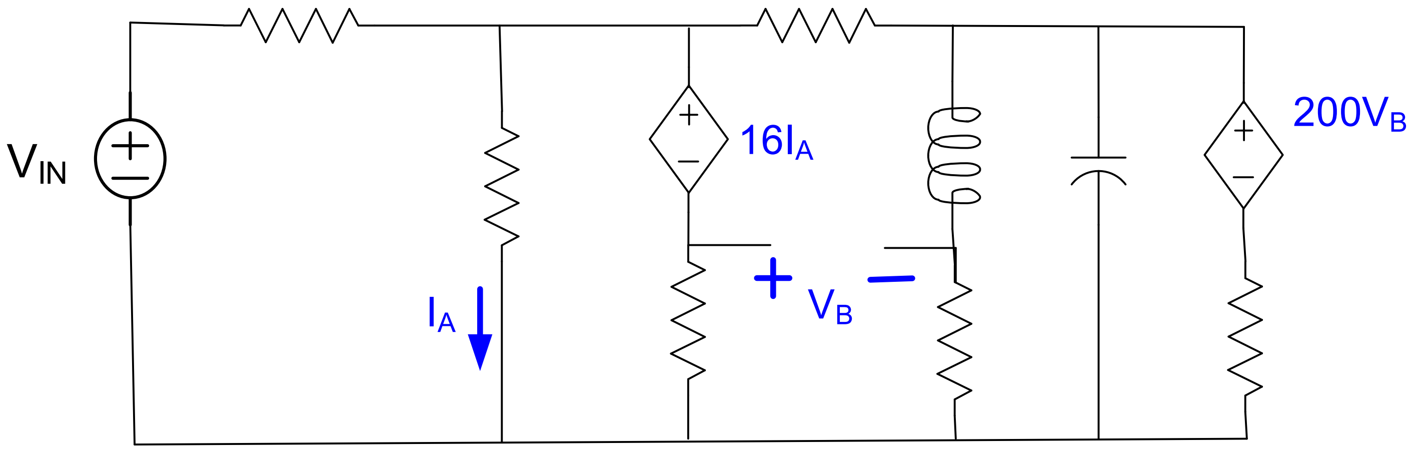
$A_V \cong -215$ $\qquad$ $R_{IN} \cong r_\pi = 930\Omega$ $\qquad$ $R_{OUT} \cong R_2 = 2K$

This is the same basic amplifier that was considered many times

Relationship with Dependent Sources ?

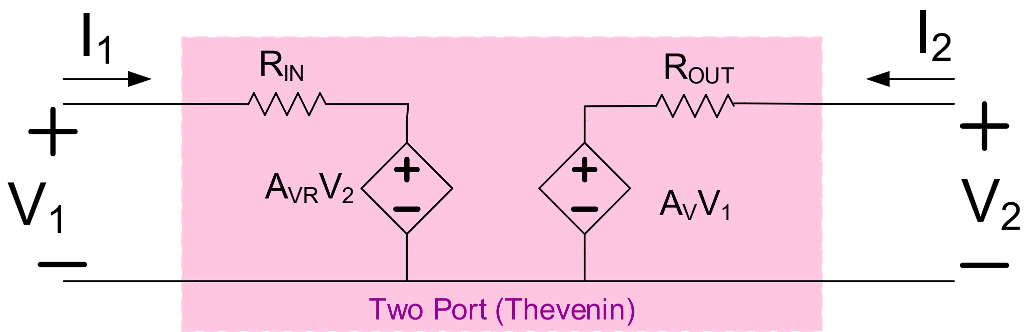


Dependent sources from EE 201



Example showing two dependent sources

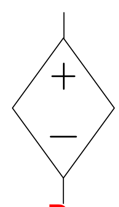
Relationship with Dependent Sources ?



Dependent sources from EE 201

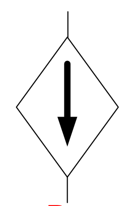
Voltage Amplifier

$v_s=\mu v_x$



Voltage Dependent Voltage Source

$I_s=\alpha v_x$

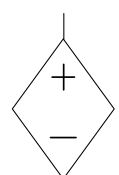


Voltage Dependent Current Source

Transconductance Amplifier

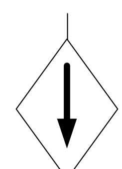
Transresistance Amplifier

$v_s=\rho I_x$



Current Dependent Voltage Source

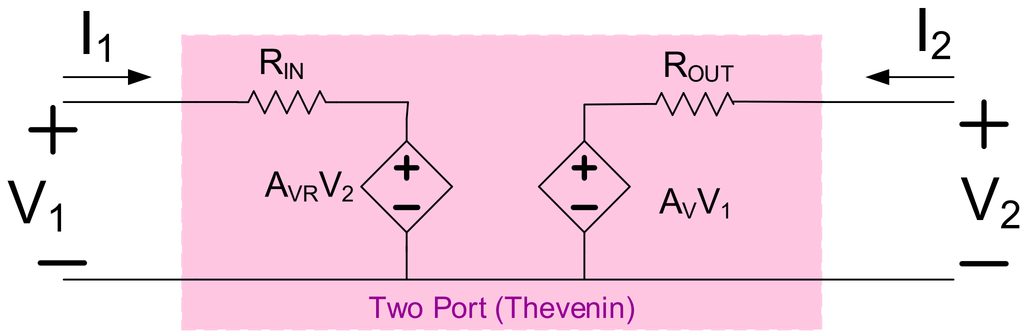
$I_s=\beta I_x$



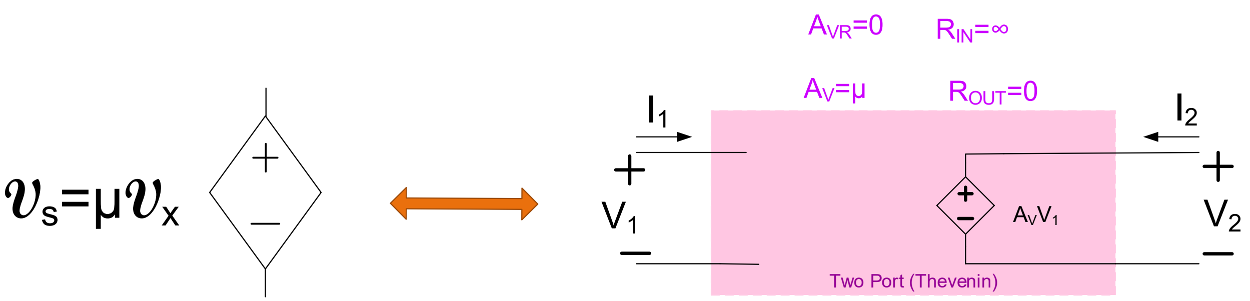
Current Dependent Current Source

Current Amplifier

Relationship with Dependent Sources ?



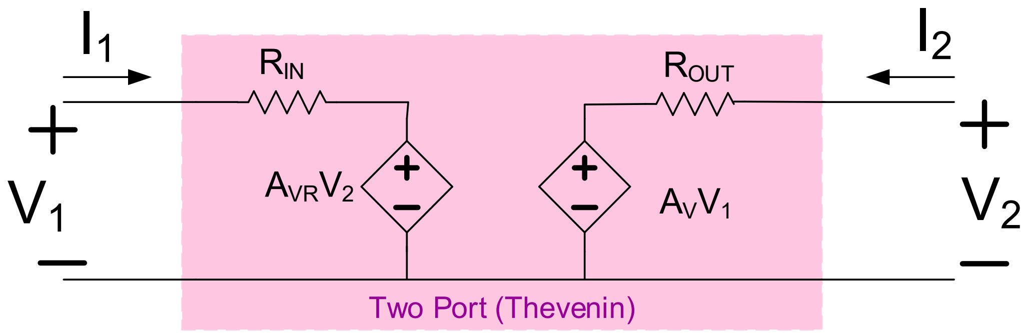
It follows that



$$V_2 = A_V V_1$$

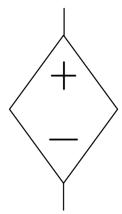
Voltage dependent voltage source is a unilateral floating two-port voltage amplifier with $R_{IN}=\infty$ and $R_{OUT}=0$

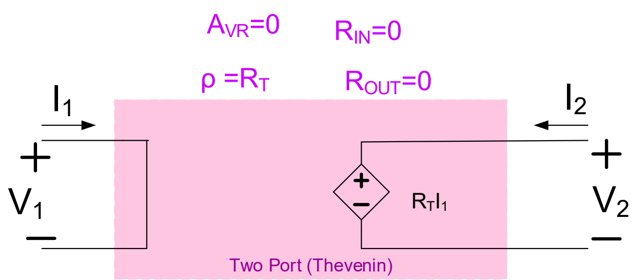
Relationship with Dependent Sources ?



It follows that

$\mathcal{v}_s=\rho I_x$

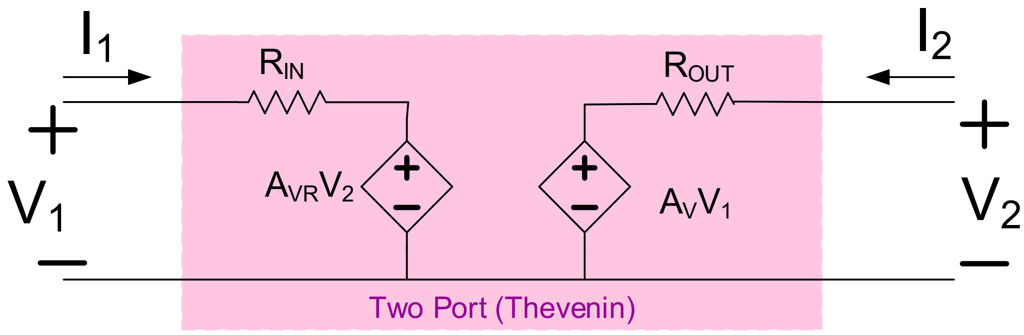




$V_2=R_TI_1$

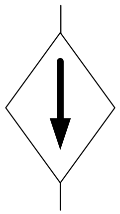
Current dependent voltage source is a unilateral floating two-port transresistance amplifier with $R_{IN}=0$ and $R_{OUT}=0$

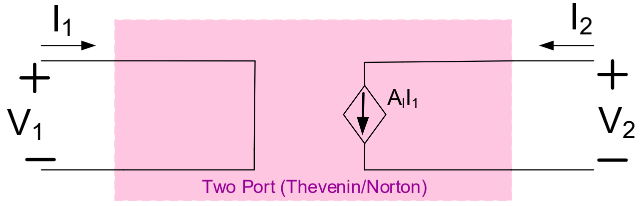
Relationship with Dependent Sources ?



It follows that

$I_S = \beta I_X$

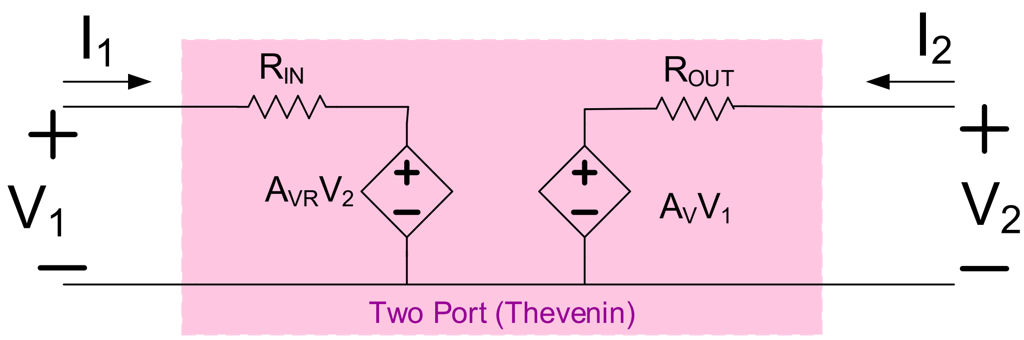




$I_2 = A_I I_1$

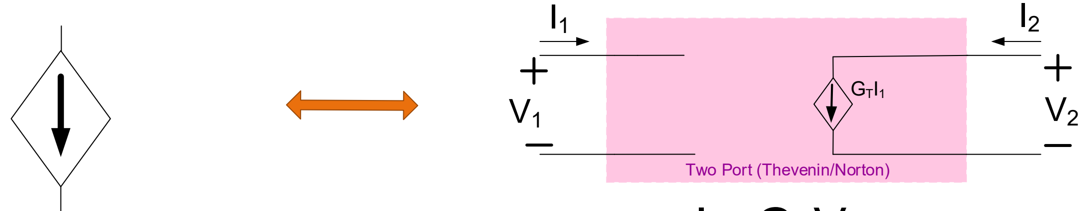
Current dependent current source is a floating unilateral two-port current amplifier with $R_{IN}=0$ and $R_{OUT}=\infty$

Relationship with Dependent Sources ?



It follows that

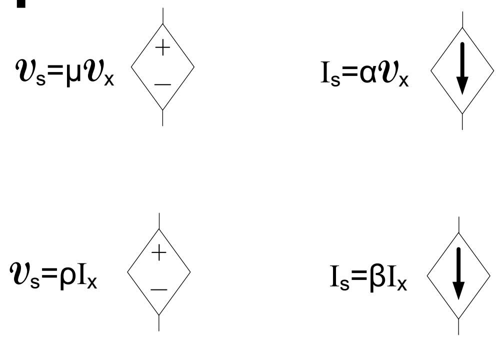
$I_s = \alpha v_x$



$I_2 = G_T V_1$

Voltage dependent current source is a floating unilateral two-port transconductance amplifier with $R_{IN}=\infty$ and $R_{OUT}=\infty$

Dependent Sources



Dependent sources are unilateral two-port amplifiers with ideal input and output impedances

Dependent sources do not exist as basic circuit elements but amplifiers can be designed to perform approximately like a dependent source

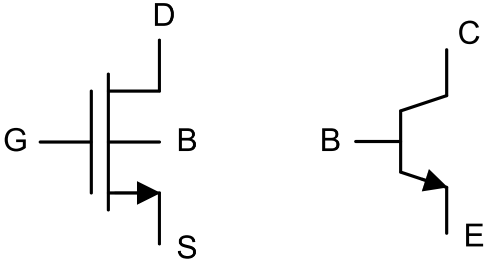
- Practical dependent sources typically are not floating on input or output
- One terminal is usually grounded
- Input and output impedances of realistic structures are usually not ideal

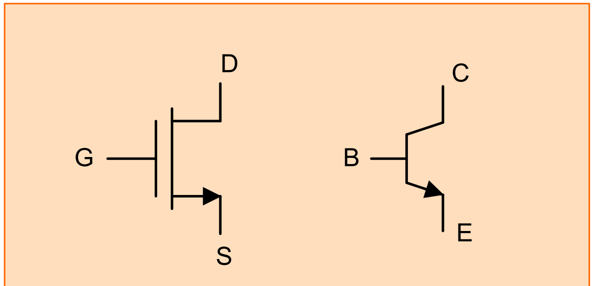
Why were "dependent sources" introduced as basic circuit elements instead of two-port amplifiers in the basic circuits courses???

Why was the concept of "dependent sources" not discussed in the basic electronics courses???

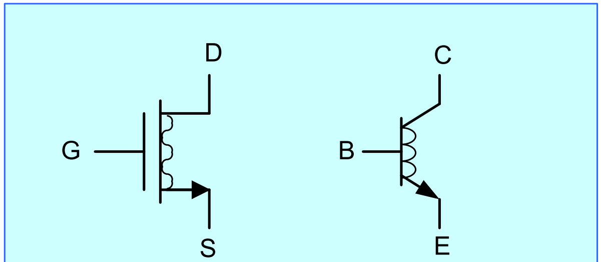
Basic Amplifier Structures

- MOS and Bipolar Transistors both have 3 primary terminals
- MOS transistor has a fourth terminal that is generally considered a parasitic terminal





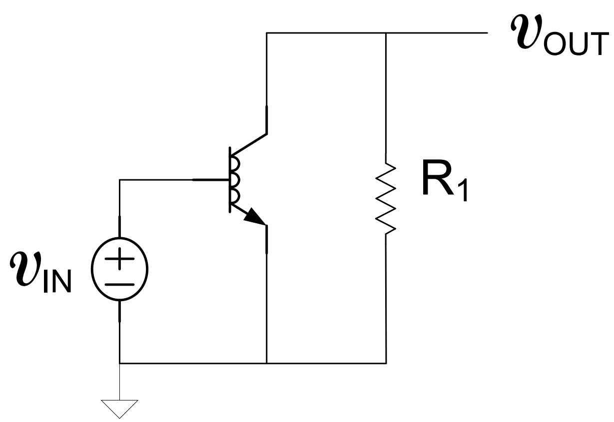
Transistors as 3-terminal Devices

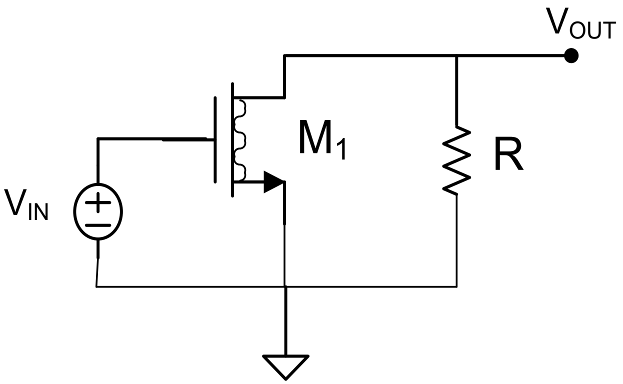


Small Signal Transistor Models
as 3-terminal Devices

Basic Amplifier Structures

Observation:



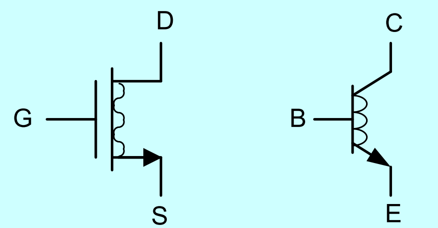


These circuits considered previously have a terminal (emitter or source) common to the input and output in the small-signal equivalent circuit

For BJT, E is common, input on B, output on C Termed "Common Emitter"

For MOSFET, S is common, input on G, output on D Termed "Common Source"

Basic Amplifier Structures



Small Signal Transistor Models
as 3-terminal Devices

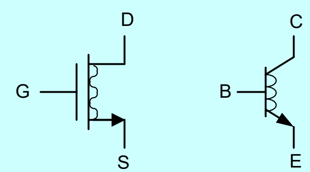
Amplifiers using these devices generally have one terminal common and use remaining terminals as input and output

Since devices are nearly unilateral, designation of input and output terminals is uniquely determined

Three different ways to designate the common terminal

Source or Emitter	termed Common Source or Common Emitter
Gate or Base	termed Common Gate or Common Base
Drain or Collector	termed Common Drain or Common Collector

Basic Amplifier Structures



	MOS			BJT		
	Common	Input	Output	Common	Input	Output
Common Source or Common Emitter	S	G	D	E	B	C
Common Gate or Common Base	G	S	D	B	E	C
Common Drain or Common Collector	D	G	S	C	B	E

Identification of Input and Output Terminals is not arbitrary

It will be shown that all 3 of the basic amplifiers are useful !

Stay Safe and Stay Healthy !

End of Lecture 28